# Fugitive Emission Calculations for WARP at 11A Pipestill

LDAR Program: Monitoring per Consent Decree<sup>1</sup>;

Factor Type: Refinery

Refinery
Screening
(EPA Emission Factors EPA-453/R-95-017, Table 2-6)

Annual Hours of Service: 8760

Component Type	Estimated Component Count	EPA 'Refinery Screening' Factors LEAK (lb/hr/component)	EPA 'Refinery Screening' Factors NO LEAK (lb/hr/component)	Percent Leak	Maximum Uncontrolled Emission Rate (lbs/hr)	LD&R Control Efficiency <sup>2</sup>	Percent in VOC Service	Total VOC Emissions (Tons/yr)
Valves								
Gas/Vapor	5	0.5789	0.0013	2.0%	0.0643	95%	100%	0.01
Light Liquid	90	0.1878	0.0037	2.0%	0.6644	95%	100%	0.15
Heavy Liquid	7	0.00051	0.00051	2.0%	0.0036	30%	100%	0.01
Pumps								
Light Liquid	1	0.9630	0.0265	2.0%	0.0452	80%	100%	0.04
Heavy Liquid	0	0.8565	0.02976	2.0%	0.0000	30%	100%	0.00
Flanges								
Gas/Vapor	15	0.0827	0.00013	0.3%	0.0057	30%	100%	0.02
Light Liquid	163	0.0827	0.00013	0.3%	0.0616	30%	100%	0.19
Heavy Liquid	12	0.0827	0.00013	0.3%	0.0045	30%	100%	0.01
Compressors	0	3.545	0.1971	2.0%	0.0000	0%	100%	0.00
Relief Valves - Added <sup>3</sup>	1	3.728	0.0985	2.0%	0.1711	98%	100%	0.01
Open-ended Lines	0	0.02635	0.0033	2.0%	0.0000	0%	100%	0.00
Sampling Connections	0	0.0827	0.00013	2.0%	0.0000	0%	100%	0.00
			Total VC	C Emission	ns Associated with	Added Componer	nts (tons/yr):	0.45

Valves									
	Gas/Vapor	0	0.5789	0.0013	2.0%	0.0000	95%	100%	0.00
	Light Liquid	-23	0.1878	0.0037	2.0%	-0.1698	95%	100%	-0.04
	Heavy Liquid	-8	0.00051	0.00051	2.0%	-0.0041	30%	100%	-0.01
Flanges									
	Gas/Vapor	0	0.0827	0.00013	0.3%	0.0000	30%	100%	0.00
	Light Liquid	-46	0.0827	0.00013	0.3%	-0.0174	30%	100%	-0.05
	Heavy Liquid	-19	0.0827	0.00013	0.3%	-0.0072	30%	100%	-0.02
				Total VOC	Fmissions	Associated with Re	moved Compone	nts (tons/vr)	-0.12

Past Emissions from Relief Valves -								
Existing Controlled <sup>3</sup>	47	3.728	0.0985	2.0%	8.0412	90%	100%	3.52
Relief Valves - Existing Controlled <sup>3</sup>	47	3.728	0.0985	2.0%	8.0412	98%	100%	0.70
Emissions Reduction (Future - Past)								-2.82
Total VOC Emissions Associated with	Added Compo	nents and Additional C	ontrols (tons/vr)					-2 50

<sup>&</sup>lt;sup>1</sup> United States, et.al v. BP Exploration & Oil, et.al., Northern District of Indiana, Hammond Division, Civil Action No. 2:96 CV 095 RL

<sup>&</sup>lt;sup>2</sup> LD&R control efficiency for pumps and valves in gas and light liquid service are 95% and 80%, respectively based on a 500 ppmv leak definition for valves and 2000 ppmv compared to the 10,000 leak definition basis for screening factors (i.e., (1-500/10,000 = 95%) and (1-2,000/10,000) = 80%)

 $<sup>\</sup>label{eq:avolution} \text{AVO monitoring equivalent to 30\% control is applied to all flanges and heavy liquid valves and pumps.}$ 

<sup>30%</sup> control estimate per TCEQ Guidance "Air Permit Technical Guidance for Chemical Sources: Equipment Leak Fugitives" (October 2000).

<sup>&</sup>lt;sup>3</sup> There is 1 new relief valve and 47 existing RV's - previously routed to the atmosphere (through the blowdown stack) that are now routed to the DDU flare. The existing RVs were previously controlled with a water spray chamber that is presumed to be capable of 90% control.

# Increased Sewer Emissions from 11A WARP Project due to Added Equipment

# **EQUIPMENT TYPE**

11A PS - Estimated Counts

EQUI MENT THE	TIATO-Lau
Atmospheric Drain Hub	15
Catch Basin (Pad or Paving Drain)	6
Inspection Points	7
Cleanouts	6
Above Ground Sewer Pump Out Points	
Sum of Drains	34
Manhole/Junction Box w/o Vent	
Manhole/Junction Box w/ CC and/or Vent	
OSBL Manholes Per Unit - Sealed	
Flare / Degassing/ KO Tanks (ie Above Ground Junction Boxes)	0
Sealed cover sumps - Gas Traps or other sumps	
Total Manholes/Junction Boxes/Sealed Sumps	0
Below Grade Oily Water Separator - Fixed Roof	
Below Grade Oily Water Separator - Floating Roof	
OSBL Sumps/OWS Per Unit	
Total In ground OWS/Sumps	0
Tanks DGO / LGO / Sour Water service	
Above Ground Oil Water Separator Tanks	
Total Above Ground Tanks	0

Does Not include Above ground pump out lines as are typically fugitive emissions included with fugitives

Assumptions:

All units will meet Benzene Neshaps Compliance Standards
No COV's will be utilized

BP Products North America, Inc. - Whiting Business Unit

		Γ			Total
			Em	ission Factor	Emissions
AP-42 Factors - Section 5-1 Petroleum Refining 1/95 - Calculations assume 50% control or drains versus uncontrolled drain emissions in AP-42	n No. of Units	Units of 1000 liters of flow	Value	Units	(kg/hr)
EMISSION INCREASES	11.01.01.01.11.10	0		· · · · · ·	(9,)
Drains Controlled	34		0.3	kg/day/unit	0.49
Junction Boxes/Manholes Controlled (Carbon Canister to comply with BWON)	0		0.03	kg/day/unit	0.00
Sealed Manholes	0		0.16	kg/day/unit	0.00
Oil Water Separator and Auxillaries				<u>Jeneraly en e</u>	
OWS	0		0.024	kg/1000 liters flow	0.000
Slop oil tanks/OW surge tanks				Use Tanks Program	0.00
OWS Abv Gr (API) Controlled	0		0.024	kg/1000 liters flow	0.000
Subtotal for Emission Increases					0.49
EMISSION DECREASES					
Area Drains Controlled			0.3	kg/day/unit	0.00
Area Drains Uncontrolled			0.7	kg/day/unit	0.00
Process Drains Controlled			0.3	kg/day/unit	0.00
Process Drains Uncontrolled			0.7	kg/day/unit	0.00
Catch Basins Controlled			0.3	kg/day/unit	0.00
Catch Basins Uncontrolled			0.7	kg/day/unit	0.00
Junction Boxes/Manholes Controlled (Carbon Canister to comply with BWON)			0.03	kg/day/unit	0.00
Sealed Manholes			0.16	kg/day/unit	0.00
Junction Boxes/Manholes Uncontrolled			0.7	kg/day/unit	0.00
Oil Water Separator and Auxillaries				<u> </u>	
OWS (API) Controlled			0.024	kg/1000 liters	0.00
OWS (API) Uncontrolled			0.6	kg/1000 liters	0.00
Slop oil tanks/OW surge tanks				<u> </u>	0.00
OWS Abv Gr (API) UnControlled			0.6	kg/1000 liters	0.00
OWS Abv Gr (API) Controlled			0.024	kg/1000 liters	0.00
Subtotal for Emission Decreases					0.00
NET EMISSIONS				kg/hr	0.49
				lb/d	25.89
				lb/yr	9451
				TPY	4.7

#### Notes:

140103.			
Emission Source		Units	Source*
			AP-42 (e.g.
Uncontrolled Drain	0.69	Kg/day	450/650)
Controlled Drain (with water trap – 50% control of AP-			
42)	0.0145		BIDa
Sealed Manway Cover (gasketed – 77% of AP-42)	0.022	Kg/hr	BIDb
Uncontrolled Junction Box (same as an Uncontrolled			AP-42 (ref.
Drain)	0.029	Kg/hr	BIDa)
Controlled Junction Box (with carbon canister to			
comply with BWON – 5% of AP-42)	0.00145	Kg/hr	BIDa, BWON
		Kg/1000	
Uncontrolled OWS	0.6	liters	AP-42
		Kg/1000	
Controlled OWS	0.024	liters	AP-42

### \*Notes:

BIDa - Background Information Document to Proposed NSPS QQQ, Feb. 1985.

BIDb - Background Information Document to Proposed NSPS QQQ, Dec. 1987.

AP-42 - AP 42, Fifth Edition, Volume I Chapter 5.1 Petroleum Refining, Jan. 1995.

Process			HHV	Sulfur	Frequency	Duration		VOC			1	IO <sub>X</sub>			SO <sub>2</sub>				PM			PM <sub>1</sub>	/PM <sub>2.5</sub>			С	0				Pb			Hg				Ве	
Unit	Malfur	nction Rates	BTU/scf	ppm	#/year	hours	EF	Unit lb/event	tpy	EF	Unit	lb/event1	tpy	EF Unit	lb/event1	tpy	EF	Unit	lb/event1	tpy	EF	Unit	lb/event1	tpy	EF	Unit	lb/event1	tpy	EF	Unit	lb/event1	tpy	EF Unit	lb/day1	tpy	EF	Unit	lb/day1	tpy
AZ-29	0.2466	MMscfh	4,420	1,000	2.0	0.33				0.068	lb/MMBtu	24.7	0.02	see below2	13.7	0.01	1.9	lb/MMscf	0.68	0.00	7.6	lb/MMscf	2.71	0.00	0.37	lb/MMBtu	134.4	0.13	5.0E-04	lb/MMscf	1.8E-04	1.78E-07	1.84E-04 lb/MMscf	6.5E-05	6.54E-08	1.20E-05	lb/MMscf	4.3E-06	4.27E-09
AZ-509	0.0356	MMscfh	4,000	150,000	1.0	0.33				0.068	lb/MMBtu	3.2	0.00	see below2	295.8	0.15	1.9	lb/MMscf	0.09	0.00	7.6	lb/MMscf	0.35	0.00	0.37	lb/MMBtu	17.6	0.01	5.0E-04	lb/MMscf	2.3E-05	1.16E-08	1.84E-04 lb/MMscf	8.5E-06	4.27E-09	1.20E-05	lb/MMscf	5.6E-07	2.79E-10
AZ-575/AZ-578	0.8331	MMscfh	5,060	1,000	1.0	0.33				0.068	lb/MMBtu	95.6	0.05	see below2	46.1	0.02	1.9	lb/MMscf	2.62	0.00	7.6	lb/MMscf	10.47	0.01	0.37	lb/MMBtu	519.9	0.26	5.0E-04	lb/MMscf	6.9E-04	3.44E-07	1.84E-04 lb/MMscf	2.5E-04	1.26E-07	1.20E-05	lb/MMscf	1.7E-05	8.27E-09
AZ-0589	0.1362	MMscfh	1,300	30,000	1.0	0.33				0.068	lb/MMBtu	4.0	0.00	see below2	226.3	0.11	1.9	lb/MMscf	0.11	0.00	7.6	lb/MMscf	0.44	0.00	0.37	lb/MMBtu	21.8	0.01	5.0E-04	lb/MMscf	2.9E-05	1.45E-08	1.84E-04 lb/MMscf	1.1E-05	5.31E-09	1.20E-05	lb/MMscf	6.9E-07	3.47E-10

	VOC <sup>3</sup>	NO <sub>X</sub>	SO <sub>2</sub>	PM		PM <sub>10</sub> /PM <sub>2.5</sub>	СО		Pb	Hg	Be
Total Projected Actual Emissions		7.6E-02	0.30	2.1	2.1E-03	8.3E-03	3	0.41	5.5E-07	2.0E-0	7 1.3E-08
Major New Source Review Thresholds	40	40	40		25	15		100	0.6	0.1	0.1
Major New Source Review Triggered?	No	No	No		No	No		No	No	No	No

<sup>1</sup> Event emission rate represents one worst case emergency/malfunction scenario event. Annual emission rate represents the estimated annual average total duration of worst case emergency/malfunction events.

<sup>2</sup>SO<sub>2</sub> Emissions Calculation:

SO2 MW (lb/lb-mole)=

64

SO2 emissions are calculated based on the concentration of sulfur in the gas stream, the ideal gas law, and the molecular weight of SO2.

General Assumptions Used in Calculations Value 1,000,000 ft^3 14.7 psia 10.73 psia-ft^3/lbmol-R 527.7 R 2596.15 lbmols/MMscf

385.1851 scf/lbmol

Ideal Gas Law used to determine the moles of gas per MSCF (P\*V=n\*R\*T)

Note that VOC emissions will actually decrease with respect to the current scenario where releases are not vented to the Flare since they will be controlled by the Flare; therefore, the potential VOC emissions associated with emergencies and malfunctions will decrease. Refer to the application text for more information.

- Other Notes:

   Natural gas Higher Heating Value (Btu/scf) = 1020

   The 11A WARP project ties existing blowdown RVs to the DDU Flare header system and consists of emergency RVs only. Nitrogen will be used as the purge gas for the new header tie-ins.

   No modifications to the flare, flare knockout drum, or piping from the knockout drum to the flare required modifications to accommodate the worst case emergency relief scenarios when considering the worst case relief scenarios for the current operations.

   Regulatory applicability for 40 CFR 63, Subpart CC will not change as a result of the project. Emergency RVs are not miscellaneous process vents per 40 CFR 63, Subpart CC since they are exempted from the definition in 40 CFR 63.641

   RV release gas combustion emission factors for PM/PM10/PM2.5, Lead, Mercury, and Beryllium are from AP-42 Section 1.4 (July 1998). Emission factors for VOC, NOx, and CO are from AP-42 Section 13.5 (September 1991). The emissions for SO2 are calculated

   The HHV and sulfur content was conservatively estimated based on the range of material that could be released. It was also conservatively assumed that each RV would lift one time per year, although this is an unlikely scenario.

# Fugitive Emission Calculations for WARP at 11C Pipestill

Note that these counts also include work to control RVs for the 11B Coker that are part of the 11C WARP Project.

LDAR Program: Monitoring per Consent Decree<sup>1</sup>;

Factor Type: Refinery

Screening (EPA Emission Factors EPA-453/R-95-017, Table 2-6)

Annual Hours of Service: 8

8760

Component Type	Estimated Component Count	EPA 'Refinery Screening' Factors LEAK (lb/hr/component)	EPA 'Refinery Screening' Factors NO LEAK (lb/hr/component)	Percent Leak	Maximum Uncontrolled Emission Rate (lbs/hr)	LD&R Control Efficiency <sup>2</sup>	Percent in VOC Service	Total VOC Emissions (Tons/yr)
Valves								
Gas/Vapor	1	0.5789	0.0013	2.0%	0.0129	95%	100%	0.00
Light Liquid	51	0.1878	0.0037	2.0%	0.3765	95%	100%	0.08
Heavy Liquid	33	0.00051	0.00051	2.0%	0.0168	30%	100%	0.05
Pumps								
Light Liquid	2	0.9630	0.0265	2.0%	0.0905	80%	100%	0.08
Heavy Liquid	0	0.8565	0.02976	2.0%	0.0000	30%	100%	0.00
Flanges								
Gas/Vapor	10	0.0827	0.00013	0.3%	0.0038	30%	100%	0.01
Light Liquid	135	0.0827	0.00013	0.3%	0.0510	30%	100%	0.16
Heavy Liquid	71	0.0827	0.00013	0.3%	0.0268	30%	100%	0.08
Compressors	0	3.545	0.1971	2.0%	0.0000	0%	100%	0.00
Relief Valves - Added <sup>3</sup>	0	3.728	0.0985	2.0%	0.0000	98%	100%	0.00
Open-ended Lines	0	0.02635	0.0033	2.0%	0.0000	0%	100%	0.00
Sampling Connections	0	0.0827	0.00013	2.0%	0.0000	0%	100%	0.00
			Total VC	C Emission	ns Associated with	Added Componer	nts (tons/yr):	0.47
Valves								
Gas/Vapor	0	0.5789	0.0013	2.0%	0.0000	95%	100%	0.00
Light Liquid	-6	0.1878	0.0037	2.0%	-0.0443	95%	100%	-0.01
Heavy Liquid	-2	0.00051	0.00051	2.0%	-0.0010	30%	100%	0.00
Flanges								
Gas/Vapor	-2	0.0827	0.00013	0.3%	-0.0008	30%	100%	0.00
Light Liquid	-34	0.0827	0.00013	0.3%	-0.0128	30%	100%	-0.04
Heavy Liquid	-7	0.0827	0.00013	0.3%	-0.0026	30%	100%	-0.01
			Total VOC	Emissions	Associated with Rer	noved Compone	nts (tons/yr):	-0.06
Past Emissions from Relief Valves -								
Existing Controlled <sup>3</sup>	77	3.728	0.0985	2.0%	13.1739	90%	100%	5.77
Relief Valves - Existing Controlled <sup>3</sup>	77	3.728	0.0985	2.0%	13.1739	98%	100%	1.15

<sup>&</sup>lt;sup>1</sup> United States, et.al v. BP Exploration & Oil, et.al., Northern District of Indiana, Hammond Division, Civil Action No. 2:96 CV 095 RL

Total VOC Emissions Associated with Added Components and Additional Controls (tons/yr):

Emissions Reduction (Future - Past)

-4.62

-4.21

<sup>&</sup>lt;sup>2</sup> LD&R control efficiency for pumps and valves in gas and light liquid service are 95% and 80%, respectively based on a 500 ppmv leak definition for valves and 2000 ppmv compared to the 10,000 leak definition basis for screening factors (i.e., (1-500/10,000 = 95%) and (1-2,000/10,000) = 80%)

 $<sup>\</sup>label{eq:avolution} \text{AVO monitoring equivalent to 30\% control is applied to all flanges and heavy liquid valves and pumps.}$ 

<sup>30%</sup> control estimate per TCEQ Guidance "Air Permit Technical Guidance for Chemical Sources: Equipment Leak Fugitives" (October 2000).

<sup>&</sup>lt;sup>3</sup> There are 2 new relief valves and 74 existing RV's - previously routed to the atmosphere (through the blowdown stack) that are now routed to the DDU flare. The existing RVs were previously controlled with a water spray chamber that is presumed to be capable of 90% control.

# Increased Sewer Emissions from 11C WARP Project due to Added Equipment UNIT

# **EQUIPMENT TYPE**

# 11C PS - Estimated Counts

Atmospheric Drain Hub	2
Catch Basin (Pad or Paving Drain)	0
Inspection Points	0
Cleanouts	0
Above Ground Sewer Pump Out Points	
Sum of Drains	2
Manhole/Junction Box w/o Vent	
Manhole/Junction Box w/ CC and/or Vent	
OSBL Manholes Per Unit - Sealed	
Flare / Degassing/ KO Tanks (ie Above Ground Junction Boxes)	0
Sealed cover sumps - Gas Traps or other sumps	
Total Manholes/Junction Boxes/Sealed Sumps	0
Below Grade Oily Water Separator - Fixed Roof	
Below Grade Oily Water Separator - Floating Roof	
OSBL Sumps/OWS Per Unit	
Total In ground OWS/Sumps	0
Tanks DGO / LGO / Sour Water service	
Above Ground Oil Water Separator Tanks	
Total Above Ground Tanks	0

Assumptions:

All units will meet Benzene Neshaps Compliance Standards
BP Products North America, Inc. - Whiting Business Unit

Does Not include Above ground pump out lines as are typically fugitive emissions included with fugitives

			_		Total
	ı	_	Emi	ssion Factor	Emissions
AP-42 Factors - Section 5-1 Petroleum Refining 1/95 - Calculations assume 50% control on drains versus uncontrolled drain emissions in AP-42	No. of Units	Units of 1000 liters of flow	Value	Units	(kg/hr)
EMISSION INCREASES					
Drains Controlled	2		0.3	kg/day/unit	0.03
Junction Boxes/Manholes Controlled (Carbon Canister to comply with BWON)	0		0.03	kg/day/unit	0.00
Sealed Manholes	0		0.16	kg/day/unit	0.00
Oil Water Separator and Auxillaries					
OWS	0		0.024	kg/1000 liters flow	0.000
Slop oil tanks/OW surge tanks				Use Tanks Program	0.00
OWS Abv Gr (API) Controlled	0		0.024	kg/1000 liters flow	0.000
Subtotal for Emission Increases					0.03
EMISSION DECREASES					
Area Drains Controlled			0.3	kg/day/unit	0.00
Area Drains Uncontrolled			0.7	kg/day/unit	0.00
Process Drains Controlled			0.3	kg/day/unit	0.00
Process Drains Uncontrolled			0.7	kg/day/unit	0.00
Catch Basins Controlled			0.3	kg/day/unit	0.00
Catch Basins Uncontrolled			0.7	kg/day/unit	0.00
Junction Boxes/Manholes Controlled (Carbon Canister to comply with BWON)			0.03	kg/day/unit	0.00
Sealed Manholes			0.16	kg/day/unit	0.00
Junction Boxes/Manholes Uncontrolled			0.7	kg/day/unit	0.00
Oil Water Separator and Auxillaries					
OWS (API) Controlled			0.024	kg/1000 liters	0.00
OWS (API) Uncontrolled			0.6	kg/1000 liters	0.00
Slop oil tanks/OW surge tanks					0.00
OWS Abv Gr (API) UnControlled			0.6	kg/1000 liters	0.00
OWS Abv Gr (API) Controlled			0.024	kg/1000 liters	0.00
Subtotal for Emission Decreases					0.00

**NET EMISSIONS** 

0.03 1.52

556

0.3

kg/hr lb/d

lb/yr

TPY

#### Notes

110100			
Emission Source		Units	Source*
			AP-42 (e.g.
Uncontrolled Drain	0.69	Kg/day	450/650)
Controlled Drain (with water trap – 50% control of AP-			
42)	0.0145	Kg/hr	BIDa
Sealed Manway Cover (gasketed – 77% of AP-42)	0.022	Kg/hr	BIDb
Uncontrolled Junction Box (same as an Uncontrolled			AP-42 (ref.
Drain)	0.029	Kg/hr	BIDa)
Controlled Junction Box (with carbon canister to			
comply with BWON – 5% of AP-42)	0.00145	Kg/hr	BIDa, BWON
		Kg/1000	
Uncontrolled OWS	0.6	liters	AP-42
		Kg/1000	
Controlled OWS	0.024	liters	AP-42

\*Notes:

BIDa - Background Information Document to Proposed NSPS QQQ, Feb. 1985.

BIDb - Background Information Document to Proposed NSPS QQQ, Dec. 1987.

AP-42 - AP 42, Fifth Edition, Volume I Chapter 5.1 Petroleum Refining, Jan. 1995.

Note that the work for 11B is associated with the 11C WARP project.

Process			HHV Su	ur Freque	ncy Dura	ition			VOC				N	O <sub>x</sub>			SO <sub>2</sub>				P	M			PM.	<sub>0</sub> /PM <sub>2.5</sub>				CO				Pb				Hg				Be	
Unit	Malfunction	Rates	BTU/scf pp	m #/yea	ar hou	ırs	EF	Unit	lb/event	it <sup>1</sup> t	ру	EF	Unit	lb/event1	tpy	EF Unit	lb/ev	ent <sup>1</sup>	tpy I	EF	Unit	lb/event1	tpy	EF	Unit	lb/event1	tpy	EF	Unit	lb/event	tpy	EF	Unit	lb/even	tpy	EF	Unit	lb/day	tpy	EF	Unit	lb/day1	tpy
C-178	0.0056525 N	MMscfh	4,000 30,	00 1.0	0.3	33						.068 lb	MMBtu	0.5	0.00	see below2	9.	4 (	0.00	1.9 lb/	/MMscf	0.01	0.00	7.6	lb/MMscf	0.06	0.00	0.37	lb/MMBtu	2.8	0.00	5.0E-	04 lb/MMsc	f 3.7E-06	1.85E-09	9 1.84E-ſ	04 lb/MMscl	1.4E-06	6.78E-10	1.20E-0	05 lb/MMscf	f 8.9E-08	4.43E-11
C-176	0.0056525 N	MMscfh	4,000 30,	00 1.0	0.3	33						.068 lb	MMBtu	0.5	0.00	see below <sup>2</sup>	9.	4 (	0.00 1	1.9 lb/	/MMscf	0.01	0.00	7.6	lb/MMscf	0.06	0.00	0.37	lb/MMBtu	2.8	0.00	5.0E-	04 lb/MMsc	f 3.7E-06	1.85E-09	∂ 1.84E-0	04 lb/MMscl	1.4E-06	6.78E-10	1.20E-0	5 lb/MMscf	f 8.9E-08	4.43E-11
C-34B	0.0157137 N	MMscfh	4,000 30,	00 1.0	0.3	33						.068 lb	MMBtu	1.4	0.00	see below <sup>2</sup>	26	.1 (	0.01 1	1.9 lb/	/MMscf	0.04	0.00	7.6	lb/MMscf	0.16	0.00	0.37	lb/MMBtu	7.8	0.00	5.0E-	04 lb/MMsc	f 1.0E-05	5.14E-09	9 1.84E-0	04 lb/MMscl	3.8E-06	1.89E-09	1.20E-0	5 lb/MMscf	2.5E-07	1.23E-10
C-220	0.0381619 N	MMscfh	4,000 30,	00 1.0	0.3	33						.068 lb	MMBtu	3.5	0.00	see below2	63	.4 (	0.03 1	1.9 lb/	/MMscf	0.09	0.00	7.6	lb/MMscf	0.38	0.00	0.37	lb/MMBtu	18.8	0.01	5.0E-	04 lb/MMsc	f 2.5E-05	1.25E-0	8 1.84E-0	04 lb/MMscl	9.2E-06	4.58E-09	1.20E-0	05 lb/MMscf	f 6.0E-07	2.99E-10
C-199	0.0022759 N	MMscfh	4,000 30,	00 1.0	0.3	33						.068 lb	MMBtu	0.2	0.00	see below <sup>2</sup>	3.	В (	0.00 1	1.9 lb/	/MMscf	0.01	0.00	7.6	lb/MMscf	0.02	0.00	0.37	lb/MMBtu	1.1	0.00	5.0E-	04 lb/MMsc	f 1.5E-06	7.44E-10	0 1.84E-0	04 lb/MMscl	5.5E-07	2.73E-10	1.20E-0	05 lb/MMscf	f 3.6E-08	1.79E-11
C-191	0.0008182 N	MMscfh	4,000 30,	00 1.0	0.3	33						.068 lb	MMBtu	0.1	0.00	see below2	1.	4 (	0.00	1.9 lb/	/MMscf	0.00	0.00	7.6	lb/MMscf	0.01	0.00	0.37	lb/MMBtu	0.4	0.00	5.0E-	04 lb/MMsc	f 5.3E-07	2.67E-10	J 1.84E-0	04 lb/MMscl	2.0E-07	9.82E-11	1.20E-0	5 lb/MMscf	1.3E-08	6.42E-12
C-194	0.0055694 N	MMscfh	4,000 30,	00 1.0	0.3	33						.068 lb	MMBtu	0.5	0.00	see below <sup>2</sup>	9.	3 (	0.00 1	1.9 lb/	/MMscf	0.01	0.00	7.6	lb/MMscf	0.06	0.00	0.37	lb/MMBtu	2.7	0.00	5.0E-	04 lb/MMsc	f 3.6E-06	1.82E-09	∂ 1.84E-0	04 lb/MMscl	1.3E-06	6.68E-10	1.20E-0	5 lb/MMscf	8.7E-08	4.37E-11
C-192	0.0055694 N	MMscfh	4,000 30,	00 1.0	0.3	33						.068 lb	MMBtu	0.5	0.00	see below <sup>2</sup>	9.	3 (	0.00	1.9 lb/	/MMscf	0.01	0.00	7.6	lb/MMscf	0.06	0.00	0.37	lb/MMBtu	2.7	0.00	5.0E-	04 lb/MMsc	f 3.6E-06	1.82E-09	9 1.84E-0	04 lb/MMscl	1.3E-06	6.68E-10	1.20E-0	5 lb/MMscf	f 8.7E-08	4.37E-11
C-174	0.0033694 N	MMscfh	4,000 30,	00 1.0	0.3	33						.068 lb	MMBtu	0.3	0.00	see below2	5.	6 (	0.00	1.9 lb/	/MMscf	0.01	0.00	7.6	lb/MMscf	0.03	0.00	0.37	lb/MMBtu	1.7	0.00	5.0E-	04 lb/MMsc	f 2.2E-06	1.10E-09	9 1.84E-ſ	04 lb/MMscl	8.1E-07	4.04E-10	1.20E-0	05 lb/MMscf	5.3E-08	2.64E-11
C-206	0.0003182 N	MMscfh	4,000 30,	00 1.0	0.3	33						.068 lb	MMBtu	0.0	0.00	see below <sup>2</sup>	0.	5 (	0.00 1	1.9 lb/	/MMscf	0.00	0.00	7.6	lb/MMscf	0.00	0.00	0.37	lb/MMBtu	0.2	0.00	5.0E-	04 lb/MMsc	f 2.1E-07	1.04E-10	J 1.84E-0	04 lb/MMscf	7.6E-08	3.82E-11	1.20E-0	5 lb/MMscf	5.0E-09	2.50E-12
C-204	0.0018602 N	MMscfh	4,000 30,	00 1.0	0.3	33						.068 lb	MMBtu	0.2	0.00	see below2	3.	1 (	0.00	1.9 lb/	/MMscf	0.00	0.00	7.6	lb/MMscf	0.02	0.00	0.37	lb/MMBtu	0.9	0.00	5.0E-	04 lb/MMsc	f 1.2E-06	6.08E-10	J 1.84E-€	04 lb/MMscl	4.5E-07	2.23E-10	1.20E-0	05 lb/MMscf	f 2.9E-08	1.46E-11
C-122	0.0340966 N	MMscfh	4,000 30,	00 1.0	0.3	33						.068 lb	MMBtu	3.1	0.00	see below <sup>2</sup>	56	.7 (	0.03 1	1.9 lb/	/MMscf	0.08	0.00	7.6	lb/MMscf	0.34	0.00	0.37	lb/MMBtu	16.8	0.01	5.0E-	04 lb/MMsc	f 2.2E-05	1.11E-0/	3 1.84E-r	04 lb/MMscf	8.2E-06	4.09E-09	1.20E-0	5 lb/MMscf	5.3E-07	2.67E-10
C-160	0.0143992 N	MMscfh	4,000 30,	00 1.0	0.3	33						.068 lb	/MMBtu	1.3	0.00	see below2	23	.9 (	0.01 1	1.9 lb/	/MMscf	0.04	0.00	7.6	lb/MMscf	0.14	0.00	0.37	lb/MMBtu	7.1	0.00	5.0E-	04 lb/MMsc	f 9.4E-06	4.71E-09	9 1.84E-ſ	04 lb/MMscl	3.5E-06	1.73E-09	1.20E-0	05 lb/MMscf	f 2.3E-07	1.13E-10
C-205	0.0346873 N	MMscfh	4,000 30,	00 1.0	0.3	33						.068 lb	MMBtu	3.1	0.00	see below2	57	.6 (	0.03 1	1.9 lb/	/MMscf	0.09	0.00	7.6	lb/MMscf	0.34	0.00	0.37	lb/MMBtu	17.1	0.01	5.0E-	04 lb/MMsc	f 2.3E-05	1.13E-0/	8 1.84E-0	04 lb/MMscl	8.3E-06	4.16E-09	1.20E-0	5 lb/MMscf	f 5.4E-07	2.72E-10

	VOC <sup>3</sup>		NO <sub>x</sub>	SO <sub>2</sub>	PM	PM <sub>10</sub> /PM <sub>2.5</sub>	CO	Pb	Hg	Be
Total Projected Actual Emissions			7.6E-03	0.14	2.1E-04	8.4E-04	0.04	5.5E-08	2.0E-08	1.3E-09
Major New Source Review Thresholds		40	40	40	25	15	100	0.6	0.1	0.1
Major New Source Review Triggered?		No	No	No	No	No	No	No	No	No

<sup>&</sup>lt;sup>1</sup> Event emission rate represents one worst case emergency/malfunction scenario event. Annual emission rate represents the estimated annual average total duration of worst case emergency/malfunction events. <sup>2</sup>SO<sub>2</sub> Emissions Calculation:

SO2 MW (lb/lb-mole)= 64 SO2 emissions are calculated based on the concentration of sulfur in the gas stream, the ideal gas law, and the molecular weight of SO2.

				•	
General Assumption	ons Used in Ca	lculations			
Variable	Value	Units			
V	1,000,000	ft^3			
P	14.7	psia			
R	10.73	psia-ft^3/lbmol-	R		
T	527.7	R			
md	2596.15	lbmols/MMscf			
	385 1851	scf/lbmol			

Ideal Gas Law used to determine the moles of gas per MSCF (P\*V=n\*R\*T)

Note that VOC emissions will actually decrease with respect to the current scenario where releases are not vented to the Flare since they will be controlled by the Flare; therefore, the potential VOC emissions associated with emergencies and malfunctions will decrease. Refer to the application text for more information.

#### Other Notes:

- Other Notes:
   Natural gas Higher Heating Value (Btu/scf) = 1020
   The 11B WARP project ties existing blowdown RVs to the DDU Flare header system and consists of emergency RVs only. Nitrogen will be used as the purge gas for the new header tie-ins.
   No modifications to the flare, flare knockout drum, or piping from the knockout drum to the flare required modifications to accommodate the worst case emergency relief scenarios when considering the worst case relief scenarios for the current operations
   Regulatory applicability for 40 CFR 63, Subpart CC will not change as a result of the project. Emergency RVs are not miscellaneous process vents per 40 CFR 63, Subpart CC since they are exempted from the definition in 40 CFR 63.641
   RV release gas combustion emission factors for PM/PM10/PM2.5, Lead, Mercury, and Beryllium are from AP-42 Section 1.4 (July 1998). Emission factors for VOC, NOx, and CO are from AP-42 Section 13.5 (September 1991). The emissions for SO2 are calculated
   The HHV and sulfur content was conservatively estimated based on the range of material that could be released. It was also conservatively assumed that each RV would lift one time per year, although this is an unlikely scenario.

Deceses	1	HHV Sulfur	Frequency	Duration	1		VOC			N	Λ			sn.			PM				PM <sub>10</sub> /I	DM			CC			Dh		I	На			Ro	
Process Unit	Malfunction Rates	_		1	FF		lb/event <sup>1</sup>	tnv	EF		-^		EF Unit	Ib/event <sup>1</sup>	1	EF				EF	Unit	2.0				, ,,,,,,,,,,,,,,,,,,,,,,,11		FF   11-14   11-1	11	EF Unit	пу	tny	FF 11-11	De	
Z-168	0.0054585 MMscfh	BTU/scf ppm 1.300 1.000	#/year 1.0	hours 0.33	EF	Unit	lb/event	tpy	0.068		lb/event	tpy	see below <sup>2</sup>	Ib/event	<b>tpy</b>	10 lb	Unit Ib	/event	tpy	7.6	Unit lb/MMscf	b/event	<b>tpy</b> 0.00	EF 0.27	Unit h/MMRtu	ib/event	tpy		event tpy 2E-06 5.80E-10	EF Unit 1.84E-04 lb/MMs			EF Unit		tpy 1.39E-11
Z-100 Z-203	0.0054565 MMscfh	1,300 1,000	1.0	0.33					0.068		0.2	0.00	see below	0.3	0.00	1.9 10	/NANAssf	0.0	0.00	7.6	lb/MMscf	0.0	0.00	0.37	b/MMRtu	0.9	0.00	O.O.E. O.I. ID/IVIIVIOOI II.	7E-07 2.84E-10	1.84E-04 lb/MMs			.20E-05 lb/MMs		6.82E-12
Z-203 Z-242	0.0026753 MMscfh	1,300 1,000	1.0	0.33					0.068		0.1	0.00	see below	0.1	0.00	1.9 ID	/MMccf	0.0	0.00	7.0	Ib/MMacf	0.0	0.00	0.01	b/MMRtu	1.0	0.00		BE-06 6.58E-10	1.84E-04 lb/MMs			.20E-05 lb/MMs		1.58E-11
Z-242 Z-154	0.0045804 MMscfh	1,300 1,000	1.0	0.33					0.068		0.2	0.00	see below <sup>2</sup>	0.3	0.00	1.9 10	/MANAgef	0.0	0.00	7.6	Ib/Mivisci	0.0	0.00	0.37	h/MMRtu	0.7	0.00	5.0E-04 ID/MINISCI 1.	7E 07 4 06E 40	1.84E-04 lb/MMs	4.0E-07 2.	705 10 1.	20E-05 lb/MMs		1.17E-11
Z-154 Z-145	0.0102079 MMscfh	1,300 1,000	1.0	0.33					0.068		0.1	0.00	see below	0.3	0.00	1.9 10	/NANAssf	0.0	0.00	7.6	lb/MMscf	0.0	0.00	0.37	b/MMBtu	0.7	0.00	5.0E-04 ID/MINISCI 9.	2E-06 1.08E-09	1.84E-04 lb/MMs	3.0E-07 1.	79E-10 1.	.20E-05 lb/MMs		2.60E-11
Z-145 Z-205	0.0102079 MMscfh	1,300 1,000	1.0	0.33					0.068		0.3	0.00	see below	0.6	0.00	1.9 ID	/MMccf	0.0	0.00	7.6	lb/MMscf	0.0			b/MMBtu	0.6	0.00		3E-06 1.06E-08	1.84E-04 lb/MMs			.20E-05 lb/MMs		7.54E-12
Z-203 Z-237	0.0029595 MMscfh	1,300 1,000	1.0	0.33					0.068		0.1	0.00	see below <sup>2</sup>	0.2	0.00	1.9 ID	/MMacf	0.0	0.00	7.6	Ib/MMacf	0.0	0.00		h/MMRtu	0.5	0.00	5.0E-04 ID/MMscf 6:	DE 07 3.14E-10	1.84E-04 lb/MMs					7.54E-12
Z-140	0.2226303 MMscfh	1,300 1,000	1.0	0.33					0.068		6.6	0.00	see below	12.3	0.00	1.9 ID	MMecf	0.0	0.00	7.6	Ib/MMecf	0.0	0.00	0.37	b/MMRtu	35.7	0.00	5.0E-04 ID/MMscf 4	7F-05 2 36F-08	1.84E-04 lb/MMs			.20E-05 lb/MMs		5.67E-10
Z-140 Z-218	0.302738 MMscfh	1,300 1,000	1.0	0.33					0.068	Dimmora	8.9	0.00	see below <sup>2</sup>	16.8	0.01	1.0 lb	/MMecf	0.2	0.00	7.6	lb/MMscf	1.0	0.00	0.37	b/MMBtu	48.5	0.02	O.OL O. ID/IVIIVIOOI I.	E 00 E:00E 00	1.84E-04 lb/MMs			20E-05 lb/MMs		0.00
Z-217	0.0102227 MMscfh	1,300 1,000	1.0	0.33					0.068		0.3	0.00	see below	0.6	0.01	1.0 lb	/MMecf	0.2	0.00	7.6	lb/MMscf	0.0	0.00		h/MMRtu	1.6	0.02	5.0E-04 lb/MMscf 2:	PE-06 1.00E-00	1.84E-04 lb/MMs					
Z-216	0.0069113 MMscfh	1,300 1,000	1.0	0.33			1	1	0.068		0.3	0.00	see below	0.0	0.00	1.9 lb	/MMscf	0.0	0.00	7.6	lb/MMscf	0.0	0.00	0.37	h/MMRtu	1.0	0.00	U.UL UT ID/IVIIVISUI Z.	5E-06 7.34E-10	1.84E-04 lb/MMs			.20E-05 lb/MMs	0.22 00	1.76E-11
Z-221	0.0094034 MMscfh	1,300 1,000	1.0	0.33					0.068		0.3	0.00	see below <sup>2</sup>	0.5	0.00	1.0 lb	/MMscf	0.0	0.00	7.6	lb/MMscf	0.0	0.00	0.37	h/MMRtu	1.5	0.00			1.84E-04 lb/MMs			20E-05 lb/MMs		
Z-207	0.0054217 MMscfh	1.300 1.000	1.0	0.33					0.068		0.2	0.00	see below <sup>2</sup>	0.3	0.00	1.9 lb	/MMscf	0.0	0.00	7.6	lb/MMscf	0.0	0.00	0.37	b/MMBtu	0.9	0.00		2E-06 5.76E-10	1.84E-04 lb/MMs					1.38E-11
Z-202	0.0045351 MMscfh	1.300 1.000	1.0	0.33					0.068	b/MMBtu	0.1	0.00	see below <sup>2</sup>	0.3	0.00	1.9 lb	/MMscf	0.0	0.00	7.6	lb/MMscf	0.0	0.00	0.37	b/MMBtu	0.7	0.00		6E-07 4.82E-10	1.84E-04 lb/MMs			20E-05 lb/MMso		1.16E-11
Z-225	0.007647 MMscfh	1,300 1,000	1.0	0.33					0.068	b/MMBtu	0.2	0.00	see below2	0.4	0.00	1.9 lb	/MMscf	0.0	0.00	7.6	lb/MMscf	0.0	0.00	0.37	b/MMBtu	1.2	0.00	5.0E-04 lb/MMscf 1.0	6E-06 8.12E-10	1.84E-04 lb/MMs	f 6.0E-07 2.	.98E-10 1.	20E-05 lb/MMso	f 3.9E-08	1.95E-11
Z-204	0.0057253 MMscfh	1,300 1,000	1.0	0.33					0.068	b/MMBtu	0.2	0.00	see below2	0.3	0.00	1.9 lb	/MMscf	0.0	0.00	7.6	lb/MMscf	0.0	0.00	0.37	b/MMBtu	0.9	0.00	5.0E-04 lb/MMscf 1.3	2E-06 6.08E-10	1.84E-04 lb/MMs	f 4.5E-07 2.	.23E-10 1.	.20E-05 lb/MMso	f 2.9E-08	1.46E-11
Z-228	0.202389 MMscfh	1,300 400,000	1.0	0.33					0.068	b/MMBtu	6.0	0.00	see below2	4483.7	2.24	1.9 lb	/MMscf	0.2	0.00	7.6	lb/MMscf	0.7	0.00	0.37	b/MMBtu	32.4	0.02	5.0E-04 lb/MMscf 4.3	BE-05 2.15E-08	1.84E-04 lb/MMs	f 1.6E-05 7.	.89E-09 1.	.20E-05 lb/MMsd	f 1.0E-06	5.16E-10
Z-139	0.0091026 MMscfh	1,300 1,000	1.0	0.33					0.068	b/MMBtu	0.3	0.00	see below2	0.5	0.00	1.9 lb	/MMscf	0.0	0.00	7.6	lb/MMscf	0.0	0.00	0.37	b/MMBtu	1.5	0.00	5.0E-04 lb/MMscf 1.9	9E-06 9.67E-10	1.84E-04 lb/MMs	f 7.1E-07 3.	.55E-10 1.	.20E-05 lb/MMso	f 4.6E-08	2.32E-11
Z-241	0.0029595 MMscfh	1,300 1,000	1.0	0.33					0.068	b/MMBtu	0.1	0.00	see below2	0.2	0.00	1.9 lb	/MMscf	0.0	0.00	7.6	lb/MMscf	0.0	0.00	0.37 I	b/MMBtu	0.5	0.00	5.0E-04 lb/MMscf 6.3	3.14E-10	1.84E-04 lb/MMs	of 2.3E-07 1.	.15E-10 1.	.20E-05 lb/MMsd	f 1.5E-08	7.54E-12
Z-101	0.2560707 MMscfh	1,300 30,000	1.0	0.33					0.068	b/MMBtu	7.5	0.00	see below2	425.5	0.21	1.9 lb	/MMscf	0.2	0.00	7.6	lb/MMscf	0.8	0.00	0.37 I	b/MMBtu	41.1	0.02	5.0E-04 lb/MMscf 5.4	1E-05 2.72E-08	1.84E-04 lb/MMs	of 2.0E-05 9.	.99E-09 1.	.20E-05 lb/MMsd	f 1.3E-06	6.53E-10
Z-107	0.8227902 MMscfh	4,496 1,000	1.0	0.33					0.068	b/MMBtu	83.9	0.04	see below <sup>2</sup>	45.6	0.02	1.9 lb	/MMscf	2.3	0.00	7.6	lb/MMscf	9.2	0.00	0.37 I	b/MMBtu	456.3	0.23	5.0E-04 lb/MMscf 6.0	E-04 3.02E-07	1.84E-04 lb/MMs	f 2.2E-04 1.	.11E-07 1.	.20E-05 lb/MMs	f 1.5E-05	7.25E-09
Z-222	0.002347 MMscfh	1,300 1,000	1.0	0.33					0.068		0.1	0.00	see below <sup>2</sup>	0.1	0.00	1.9 lb	/MMscf	0.0	0.00	7.6	lb/MMscf	0.0	0.00	0.37 I	b/MMBtu	0.4	0.00	5.0E-04 lb/MMscf 5.0	E-07 2.49E-10	1.84E-04 lb/MMs		.15E-11 1.	.20E-05 lb/MMs	f 1.2E-08	5.98E-12
Z-220	0.0056081 MMscfh	1,300 1,000	1.0	0.33					0.068		0.2	0.00	see below <sup>2</sup>	0.3	0.00	1.9 lb	/MMscf	0.0	0.00	7.6	lb/MMscf	0.0	0.00	0.37 I	b/MMBtu	0.9	0.00	5.0E-04 lb/MMscf 1.:	2E-06 5.96E-10	1.84E-04 lb/MMs	f 4.4E-07 2.	.19E-10 1.	.20E-05 lb/MMs	f 2.9E-08	1.43E-11
Z-114	0.0047881 MMscfh	1,300 1,000	1.0	0.33					0.068		0.1	0.00	see below <sup>2</sup>	0.3	0.00	1.9 lb	/MMscf	0.0	0.00	7.6	lb/MMscf	0.0	0.00	0.37 I	b/MMBtu	8.0	0.00	5.0E-04 lb/MMscf 1.0	E-06 5.09E-10	1.84E-04 lb/MMs	f 3.7E-07 1.	.87E-10 1.	.20E-05 lb/MMs	f 2.4E-08	1.22E-11
Z-156	0.0036926 MMscfh	1,300 1,000	1.0	0.33					0.068		0.1	0.00	see below <sup>2</sup>	0.2	0.00	1.9 lb	/MMscf	0.0	0.00	7.6	lb/MMscf	0.0	0.00	0.37 I	b/MMBtu	0.6	0.00	5.0E-04 lb/MMscf 7.8	3E-07 3.92E-10	1.84E-04 lb/MMs			.20E-05 lb/MMs		9.41E-12
Z-116	0.0104647 MMscfh	1,300 1,000	1.0	0.33					0.068		0.3	0.00	see below <sup>2</sup>	0.6	0.00	1.9 lb	/MMscf	0.0	0.00	7.6	lb/MMscf	0.0	0.00	0.37 I	b/MMBtu	1.7	0.00	5.0E-04 lb/MMscf 2.:	2E-06 1.11E-09	1.84E-04 lb/MMs	f 8.2E-07 4.	.08E-10 1.	.20E-05 lb/MMs		
Z-134	0.0021965 MMscfh	1,300 1,000	1.0	0.33					0.068		0.1	0.00	see below <sup>2</sup>	0.1	0.00	1.9 lb	/MMscf	0.0	0.00	7.6	lb/MMscf	0.0	0.00	0.37 I	b/MMBtu	0.4	0.00	5.0E-04 lb/MMscf 4.	7E-07 2.33E-10	1.84E-04 lb/MMs	f 1.7E-07 8.		.20E-05 lb/MMs		5.60E-12
Z-121	0.2713905 MMscfh	5,662 1,000	1.0	0.33					0.068	D) IVIII D CG	34.8	0.02	see below <sup>2</sup>	15.0	0.01	1.9 lb	/MMscf	1.0	0.00	7.6	lb/MMscf	3.8	0.00	0.37 I	b/MMBtu	189.5	0.09		5E-04 1.26E-07	1.84E-04 lb/MMs					
Z-132	0.0054392 MMscfh	1,300 1,000	1.0	0.33					0.068	b/MMBtu	0.2	0.00	see below <sup>2</sup>	0.3	0.00	1.9 lb	/MMscf	0.0	0.00	7.6	lb/MMscf	0.0	0.00	0.37	b/MMBtu	0.9	0.00	5.0E-04 lb/MMscf 1.:	2E-06 5.78E-10	1.84E-04 lb/MMs	f 4.2E-07 2.	.12E-10 1.	.20E-05 lb/MMs	f 2.8E-08	1.39E-11

	VOC <sup>3</sup>	NO <sub>X</sub>	SO <sub>2</sub>		PM PM <sub>10</sub> /PM <sub>2.5</sub>	CO	Pb	Hg	Be
Total Projected Actual Emissions			0.08	2.50	0.00	0.01 0.4	5.5E-07	2.0E-07	1.3E-08
Major New Source Review Thresholds		40	40	40	25	15 100	0.6	0.1	0.1
Major New Source Review Triggered?		N	No	No	No	No No	No	No	No

<sup>&</sup>lt;sup>1</sup> Event emission rate represents one worst case emergency/malfunction scenario event. Annual emission rate represents the estimated annual average total duration of worst case emergency/malfunction events. <sup>2</sup>SO<sub>2</sub> Emissions Calculation:

SO2 MW (lb/lb-mole)= 64
SO2 emissions are calculated based on the concentration n of sulfur in the gas stream, the ideal gas law, and the molecular weight of SO2.

General Assumptions Used in Calculations Value 1,000,000 ft^3 14.7 psia 10.73 psia-ft^3/lbmol-R 527.7 R 2596.15 lbmols/MMscf 385.1851 scf/lbmol Ideal Gas Law used to determine the moles of gas per MSCF (P\*V=n\*R\*T)

Note that VOC emissions will actually decrease with respect to the current scenario where releases are not vented to the Flare since they will be controlled by the Flare; therefore, the potential VOC emissions associated with emergencies and malfunction

Other Notes.

Natural gas Higher Heating Value (Btu/scf) = 1020

- The 11C WARP project ties existing blowdown RVs to the DDU Flare header system and consists of emergency RVs only. Nitrogen will be used as the purge gas for the new header tie-ins.

No modifications to the flare, flare knockout drum, or piping from the knockout drum to the flare required modifications to accommodate the worst case emergency relief scenarios when considering the worst case relief scenarios for the current operations.

Regulatory applicability for 40 CFR 63, Subpart CC will not change as a result of the project. Emergency RVs are not miscellaneous process vents per 40 CFR 63, Subpart CC since they are exempted from the definition in 40 CFR 63.641

RV release gas combustion emission factors for PM/PM10/PM2.5, Lead, and Mercury are from AP-42 Section 1.4 (July 1998). Emission factors for VCQ, NOx, and CO are from AP-42 Section 13.5 (September 1991). The emissions for SO2 are calculated by assumin The HHV and sulfur content was conservatively estimated based on the range of material that could be released. It was also conservatively assumed that each RV would lift one time per year, although this is an unlikely scenario.

# Fugitive Emission Calculations for WARP at FCU500

Refer to application text for more information regarding FCU 500 WARP and these estimated component counts.

LDAR Program: Monitoring per Consent Decree<sup>1</sup>;

Factor Type:

Refinery Screening (EPA Emission Factors EPA-453/R-95-017, Table 2-6)

Annual Hours of Service: 8760

	Estimated Component	EPA 'Refinery Screening' Factors LEAK	EPA 'Refinery Screening' Factors NO LEAK	Percent	Maximum Uncontrolled Emission Rate	LD&R Control	Percent in VOC	Total VOC Emissions
Component Type	Component	(lb/hr/component)	(lb/hr/component)	Leak	(lbs/hr)	Efficiency <sup>2</sup>	Service	(Tons/yr)
Valves								
Gas/Vapor	0	0.5789	0.0013	2.0%	0.0000	95%	100%	0.00
Light Liquid	93	0.1878	0.0037	2.0%	0.6865	95%	100%	0.15
Heavy Liquid	4	0.00051	0.00051	2.0%	0.0020	30%	100%	0.01
Pumps								
Light Liquid	1	0.9630	0.0265	2.0%	0.0452	80%	100%	0.04
Heavy Liquid	0	0.8565	0.02976	2.0%	0.0000	30%	100%	0.00
Flanges								
Gas/Vapor	1	0.0827	0.00013	0.3%	0.0004	30%	100%	0.00
Light Liquid	192	0.0827	0.00013	0.3%	0.0725	30%	100%	0.22
Heavy Liquid	11	0.0827	0.00013	0.3%	0.0042	30%	100%	0.01
Compressors	0	3.545	0.1971	2.0%	0.0000	0%	100%	0.00
Relief Valves	0	3.728	0.0985	2.0%	0.0000	100%	100%	0.00
Open-ended Lines	0	0.02635	0.0033	2.0%	0.0000	0%	100%	0.00
Sampling Connections	0	0.0827	0.00013	2.0%	0.0000	0%	100%	0.00
					Т	otal VOC Emission	ons (tons/yr):	0.43

<sup>&</sup>lt;sup>1</sup> United States, et.al v. BP Exploration & Oil, et.al., Northern District of Indiana, Hammond Division, Civil Action No. 2:96 CV 095 RL

<sup>&</sup>lt;sup>2</sup> LD&R control efficiency for pumps and valves in gas and light liquid service are 95% and 80%, respectively based on a 500 ppmv leak definition for valves and 2000 ppmv compared to the 10,000 leak definition basis for screening factors (i.e., (1-500/10,000 = 95%) and (1-2,000/10,000) = 80%)

AVO monitoring equivalent to 30% control is applied to all flanges and heavy liquid valves and pumps.

<sup>30%</sup> control estimate per TCEQ Guidance "Air Permit Technical Guidance for Chemical Sources: Equipment Leak Fugitives" (October 2000). Relief Valves are controlled

# Increased Sewer Emissions from FCU500 WARP Project due to Added Equipment UNIT

# **EQUIPMENT TYPE**

FCU500 - Estimated Counts

EQUI MENT III E	1 CO300 - L3
Atmospheric Drain Hub	4
Catch Basin (Pad or Paving Drain)	0
Inspection Points	0
Cleanouts	0
Above Ground Sewer Pump Out Points	
Sum of Drains	4
Manhole/Junction Box w/o Vent	
Manhole/Junction Box w/ CC and/or Vent	
OSBL Manholes Per Unit - Sealed	
Flare / Degassing/ KO Tanks (ie Above Ground Junction Boxes)	0
Sealed cover sumps - Gas Traps or other sumps	
Total Manholes/Junction Boxes/Sealed Sumps	0
Below Grade Oily Water Separator - Fixed Roof	
Below Grade Oily Water Separator - Floating Roof	
OSBL Sumps/OWS Per Unit	
Total In ground OWS/Sumps	0
Tanks DGO / LGO / Sour Water service	
Above Ground Oil Water Separator Tanks	
Total Above Ground Tanks	0

Does Not include Above ground pump out lines as are typically fugitive emissions included with fugitives

Assumptions:

All units will meet Benzene Neshaps Compliance Standards
No COV's will be utilized

					Total Emission
			Em	ission Factor	s
AP-42 Factors - Section 5-1 Petroleum Refining 1/95 - Calculations assume 50% control	No. of	Units of 1000 liters			
on drains versus uncontrolled drain emissions in AP-42	Units	of flow	Value	Units	(kg/hr)
EMISSION INCREASES		-			
Drains Controlled	4		0.3	kg/day/unit	0.06
Junction Boxes/Manholes Controlled (Carbon Canister to comply with BWON)	0		0.03	kg/day/unit	0.00
Sealed Manholes	0		0.16	kg/day/unit	0.00
Oil Water Separator and Auxillaries					
OWS	0		0.024	kg/1000 liters flow	0.000
Slop oil tanks/OW surge tanks				Use Tanks Program	0.00
OWS Abv Gr (API) Controlled	0		0.024	kg/1000 liters flow	0.000
Subtotal for Emission Increases					0.06
EMISSION DECREASES					
Area Drains Controlled			0.3	kg/day/unit	0.00
Area Drains Uncontrolled			0.7	kg/day/unit	0.00
Process Drains Controlled			0.3	kg/day/unit	0.00
Process Drains Uncontrolled			0.7	kg/day/unit	0.00
Catch Basins Controlled			0.3	kg/day/unit	0.00
Catch Basins Uncontrolled			0.7	kg/day/unit	0.00
Junction Boxes/Manholes Controlled (Carbon Canister to comply with BWON)			0.03	kg/day/unit	0.00
Sealed Manholes			0.16	kg/day/unit	0.00
Junction Boxes/Manholes Uncontrolled			0.7	kg/day/unit	0.00
Oil Water Separator and Auxillaries					
OWS (API) Controlled			0.024	kg/1000 liters	0.00
OWS (API) Uncontrolled			0.6	kg/1000 liters	0.00
Slop oil tanks/OW surge tanks					0.00
OWS Abv Gr (API) UnControlled			0.024	kg/1000 liters	0.00
OWS Abv Gr (API) Controlled			0.6	kg/1000 liters	0.00
. ,				-	
Subtotal for Emission Decreases					0.00

**NET EMISSIONS** 

kg/hr	0.06
lb/d	3.05
lb/yr	1112
TPY	0.6

#### Notes:

TNOIGS.			_
Emission Source		Units	Source*
			AP-42 (e.g.
Uncontrolled Drain	0.69	Kg/day	450/650)
Controlled Drain (with water trap – 50% control of AP-			
42)	0.0145	Kg/hr	BIDa
Sealed Manway Cover (gasketed – 77% of AP-42)	0.022	Kg/hr	BIDb
Uncontrolled Junction Box (same as an Uncontrolled			AP-42 (ref.
Drain)	0.029	Kg/hr	BIDa)
Controlled Junction Box (with carbon canister to			
comply with BWON – 5% of AP-42)	0.00145	Kg/hr	BIDa, BWON
		Kg/1000	
Uncontrolled OWS	0.6	liters	AP-42
		Kg/1000	
Controlled OWS	0.024	liters	AP-42

### \*Notes:

BIDa - Background Information Document to Proposed NSPS QQQ, Feb. 1985.

BIDb - Background Information Document to Proposed NSPS QQQ, Dec. 1987.

AP-42 - AP 42, Fifth Edition, Volume I Chapter 5.1 Petroleum Refining, Jan. 1995.

# Fugitive Emission Calculations for WARP at FCU 600

LDAR Program: Monitoring per Consent Decree<sup>1</sup>;

Factor Type: Refinery

Refinery
Screening
(EPA Emission Factors EPA-453/R-95-017, Table 2-6)

Annual Hours of Service: 8760

Component Type	Estimated Component Count	EPA 'Refinery Screening' Factors LEAK (Ib/hr/component)	EPA 'Refinery Screening' Factors NO LEAK (lb/hr/component)	Percent Leak	Maximum Uncontrolled Emission Rate (lbs/hr)	LD&R Control Efficiency <sup>2</sup>	Percent in VOC Service	Total VOC Emissions (Tons/yr)
Valves								
Gas/Vapor	0	0.5789	0.0013	2.0%	0.0000	95%	100%	0.00
Light Liquid	93	0.1878	0.0037	2.0%	0.6865	95%	100%	0.15
Heavy Liquid	4	0.00051	0.00051	2.0%	0.0020	30%	100%	0.01
Pumps								
Light Liquid	1	0.9630	0.0265	2.0%	0.0452	80%	100%	0.04
Heavy Liquid	0	0.8565	0.02976	2.0%	0.0000	30%	100%	0.00
Flanges								
Gas/Vapor	1	0.0827	0.00013	0.3%	0.0004	30%	100%	0.00
Light Liquid	192	0.0827	0.00013	0.3%	0.0725	30%	100%	0.22
Heavy Liquid	11	0.0827	0.00013	0.3%	0.0042	30%	100%	0.01
Compressors	0	3.545	0.1971	2.0%	0.0000	0%	100%	0.00
Relief Valves - Added <sup>3</sup>	0	3.728	0.0985	2.0%	0.0000	98%	100%	0.00
Open-ended Lines	0	0.02635	0.0033	2.0%	0.0000	0%	100%	0.00
Sampling Connections	0	0.0827	0.00013	2.0%	0.0000	0%	100%	0.00
			Total VC	C Emission	ns Associated with	Added Componer	nts (tons/yr):	0.43

Valves								
Gas/Vapo	r 0	0.5789	0.0013	2.0%	0.0000	95%	100%	0.00
Light Liquid	-15	0.1878	0.0037	2.0%	-0.1107	95%	100%	-0.02
Heavy Liquid	d -2	0.00051	0.00051	2.0%	-0.0010	30%	100%	0.00
Flanges								
Gas/Vapo	r -6	0.0827	0.00013	0.3%	-0.0023	30%	100%	-0.01
Light Liquid	-22	0.0827	0.00013	0.3%	-0.0083	30%	100%	-0.03
Heavy Liqui	d -7	0.0827	0.00013	0.3%	-0.0026	30%	100%	-0.01
			Total VOC	Fmissions	Associated with Rea	moved Compone	nts (tons/vr):	-0.07

Past Emissions from Relief Valves -								
Existing Controlled <sup>3</sup>	41	3.728	0.0985	2.0%	7.0147	90%	100%	3.07
Relief Valves - Existing Controlled <sup>3</sup>	41	3.728	0.0985	2.0%	7.0147	98%	100%	0.61
Emissions Reduction (Future - Past)								-2.46
Total VOC Emissions Associated with	Added Compo	nents and Additional C	Controls (tons/vr):					-2.09

<sup>&</sup>lt;sup>1</sup> United States, et.al v. BP Exploration & Oil, et.al., Northern District of Indiana, Hammond Division, Civil Action No. 2:96 CV 095 RL

<sup>&</sup>lt;sup>2</sup> LD&R control efficiency for pumps and valves in gas and light liquid service are 95% and 80%, respectively based on a 500 ppmv leak definition for valves and 2000 ppmv compared to the 10,000 leak definition basis for screening factors (i.e., (1-500/10,000 = 95%) and (1-2,000/10,000) = 80%)

AVO monitoring equivalent to 30% control is applied to all flanges and heavy liquid valves and pumps.

<sup>30%</sup> control estimate per TCEQ Guidance "Air Permit Technical Guidance for Chemical Sources: Equipment Leak Fugitives" (October 2000).

<sup>&</sup>lt;sup>3</sup> There are no new relief valves and 41 existing RV's - previously routed to the atmosphere (through the blowdown stack) that are now routed to the FCU flare. The existing RVs were previously controlled with a water spray chamber that is presumed to be capable of 90% control.

# Increased Sewer Emissions from FCU600 WARP Project due to Added Equipment UNIT

# **EQUIPMENT TYPE**

FCU600 - Estimated Counts

• =		
Atmospheric Drain Hub	4	
Catch Basin (Pad or Paving Drain)	0	
Inspection Points	0	
Cleanouts	0	
Above Ground Sewer Pump Out Points		
Sum of Drains	4	
Manhole/Junction Box w/o Vent		
Manhole/Junction Box w/ CC and/or Vent	1	
OSBL Manholes Per Unit - Sealed		
Flare / Degassing/ KO Tanks (ie Above Ground Junction Boxes)	0	
Sealed cover sumps - Gas Traps or other sumps		
Total Manholes/Junction Boxes/Sealed Sumps	1	
Below Grade Oily Water Separator - Fixed Roof		
Below Grade Oily Water Separator - Floating Roof		
OSBL Sumps/OWS Per Unit		
Total In ground OWS/Sumps	0	
Tanks DGO / LGO / Sour Water service		
Above Ground Oil Water Separator Tanks		
Total Above Ground Tanks	0	
Assumptions:		

Does Not include Above ground pump out lines as are typically fugitive emissions included with fugitives

Assumptions:

All units will meet Benzene Neshaps Compliance Standards
No COV's will be utilized

					Total
			Emi	ssion Factor	<b>Emissions</b>
		Units of			
AP-42 Factors - Section 5-1 Petroleum Refining 1/95 - Calculations assume		1000 liters			
drains versus uncontrolled drain emissions in AP-42	No. of Units	of flow	Value	Units	(kg/hr)
EMISSION INCREASES					
Drains Controlled	4		0.3	kg/day/unit	0.06
Junction Boxes/Manholes Controlled (Carbon Canister to comply with BWON)	0		0.03	kg/day/unit	0.00
Sealed Manholes	0		0.16	kg/day/unit	0.00
Oil Water Separator and Auxillaries					
OWS	0		0.024	kg/1000 liters flow	0.000
Slop oil tanks/OW surge	tanks			Use Tanks Program	0.00
OWS Abv Gr (API) Con	trolled 0		0.024	kg/1000 liters flow	0.000
Subtotal for Emission Increases					0.06
EMISSION DECREASES					
Area Drains Controlled			0.3	kg/day/unit	0.00
Area Drains Uncontrolled			0.7	kg/day/unit	0.00
Process Drains Controlled			0.3	kg/day/unit	0.00
Process Drains Uncontrolled			0.7	kg/day/unit	0.00
Catch Basins Controlled			0.3	kg/day/unit	0.00
Catch Basins Uncontrolled			0.7	kg/day/unit	0.00
Junction Boxes/Manholes Controlled (Carbon Canister to comply with BWON)			0.03	kg/day/unit	0.00
Sealed Manholes			0.16	kg/day/unit	0.00
Junction Boxes/Manholes Uncontrolled			0.7	kg/day/unit	0.00
Oil Water Separator and Auxillaries				<u> </u>	
OWS (API) Controlled			0.024	kg/1000 liters	0.00
OWS (API) Uncontrolled	d d		0.6	kg/1000 liters	0.00
Slop oil tanks/OW surge				<u>J</u>	0.00
OWS Abv Gr (API) UnC			0.024	kg/1000 liters	0.00
OWS Abv Gr (API) Con			0.6	kg/1000 liters	0.00
Subtotal for Emission Decreases					0.00
NET EMISSIONS				kg/hr	0.06
				lb/d	3.05
				lb/yr	1112
				TPY	0.6

#### Notes:

Emission Source		Units	Source*
			AP-42 (e.g.
Uncontrolled Drain	0.69	Kg/day	450/650)
Controlled Drain (with water trap - 50% control of AP-			
42)	0.0145	Kg/hr	BIDa
Sealed Manway Cover (gasketed – 77% of AP-42)	0.022	Kg/hr	BIDb
Uncontrolled Junction Box (same as an Uncontrolled			AP-42 (ref.
Drain)	0.029	Kg/hr	BIDa)
Controlled Junction Box (with carbon canister to			
comply with BWON – 5% of AP-42)	0.00145	Kg/hr	BIDa, BWON
		Kg/1000	
Uncontrolled OWS	0.6	liters	AP-42
		Kg/1000	
Controlled OWS	0.024	liters	AP-42

<sup>\*</sup>Notes:

BIDa - Background Information Document to Proposed NSPS QQQ, Feb. 1985.

BIDb - Background Information Document to Proposed NSPS QQQ, Dec. 1987.

AP-42 - AP 42, Fifth Edition, Volume I Chapter 5.1 Petroleum Refining, Jan. 1995.

	1		HHV	Culfur	Eroguen	y Duration	1	- v	/OC			NO				80			<del></del>	DM			DM	<sub>0</sub> /PM <sub>2.5</sub>		CO Db						T 11=				D <sub>0</sub>					
						<u> </u>	<b></b>					,	1			3U <sub>2</sub>			<del></del>	TIVI	11			0/PIVI <sub>2.5</sub>	.11	<del> </del>	T	Ju	11 .	L		τυ Ι			<del> '</del>	1 <b>y</b>		<del>  </del>		1 T	
RV's	Malfunct		BTU/scf	ppm	#/year		EF	Unit	lb/event	tpy			lb/event	tpy	EF Unit	lb/event	tpy	EF	Unit	lb/event	tpy	EF	Unit	lb/even	t tpy	EF	Unit	lb/event	tpy	EF	Unit	lb/event	tpy	EF	Unit	lb/day	tpy	EF	Unit	lb/day1	tpy
R-0041	1.33E-03	MMscfh	14,626	12,000	1	0.33					0.068 lb		0.4	0.00	see below <sup>2</sup>	0.9	0.00	1.9	lb/MMsct	0.0	0.00	7.6	lb/MMsc	t 0.0	0.00	0.37	lb/MMBtu	2.4	0.00	5.0E-04	10/11111001		1.000		lb/MMscf	1.2E-06		1.20E-05 lb		7.6E-08	3.82E-11
R-0045	1.33E-03	MMscfh	,	12,000	1	0.33					0.068 lb	, will the	0.4	0.00	see below <sup>2</sup>	0.9	0.00	1.9	lb/MMscf	0.0	0.00	7.6	lb/MMsc	f 0.0	0.00	0.37	lb/MMBtu	2.4	0.00	5.0E-04	lb/MMscf	3.2E-06	1.59E-09	1.012 01	lb/MMscf	1.2E-06	5.85E-10	1.20E-05 lb	/MMscf		
R-0049	1.33E-03	MMscfh	,	12,000	1	0.33					0.068 lb		0.4	0.00	see below <sup>2</sup>	0.9	0.00	1.9	lb/MMsct	0.0	0.00	7.6	lb/MMsc	t 0.0	0.00	0.37	lb/MMBtu	2.4	0.00	5.0E-04	lb/MMscf	3.2E-06	1.59E-09	1.84E-04		1.2E-06	5.85E-10	1.20E-05 lb	/MMsct	7.6E-08	3.82E-11
R-0047	1.33E-03	MMscfh	,	12,000	1	0.33					0.068 lb	, will the	0.4	0.00	see below <sup>2</sup>	0.9	0.00	1.9	lb/MMscf	0.0	0.00	7.6	lb/MMsc	f 0.0	0.00	0.37	lb/MMBtu	2.4	0.00	5.0E-04	lb/MMscf	3.2E-06	1.59E-09		lb/MMscf	1.2E-06	0.00-	1.20E-05 lb		7.6E-08	3.82E-11
R-0048	1.33E-03	MMscfh	14,626	12,000	1	0.33					0.068 lb		0.4	0.00	see below2	0.9	0.00	1.9	lb/MMscf	0.0	0.00	7.6	lb/MMsc	f 0.0	0.00	0.37	lb/MMBtu	2.4	0.00	5.0E-04	lb/MMscf	3.2E-06	1.59E-09	1.84E-04	10711111001	1.2E-06	0.00	1.20E-05 lb	,	7.6E-08	3.82E-11
R-0051	1.33E-03	MMscfh	14,626	12,000	1	0.33					0.068 lb		0.4	0.00	see below <sup>2</sup>	0.9	0.00	1.9	lb/MMscf	0.0	0.00	7.6	lb/MMsc	f 0.0	0.00	0.37	lb/MMBtu	2.4	0.00	5.0E-04	lb/MMscf	3.2E-06	1.59E-09	1.84E-04		1.2E-06	5.85E-10	1.20E-05 lb	/MMscf	7.6E-08	3.82E-11
R-2099	2.52E-03	MMscfh	14,626	12,000	1	0.33					0.068 lb		8.0	0.00	see below <sup>2</sup>	1.7	0.00	1.9	lb/MMscf	0.0	0.00	7.6	lb/MMsc	f 0.1	0.00	0.37	lb/MMBtu	4.5	0.00	5.0E-04	lb/MMscf	6.0E-06	3.01E-09	1.84E-04	lb/MMscf	2.2E-06	1.10E-09	1.20E-05 lb	/MMscf	1.4E-07	7.22E-11
R-2100	2.52E-03	MMscfh	14,626	12,000	1	0.33					0.068 lb		8.0	0.00	see below <sup>2</sup>	1.7	0.00	1.9	lb/MMscf	0.0	0.00	7.6	lb/MMsc	f 0.1	0.00	0.37	lb/MMBtu	4.5	0.00	5.0E-04	lb/MMscf	6.0E-06	3.01E-09	1.84E-04	lb/MMscf	2.2E-06	1.10E-09	1.20E-05 lb	/MMscf	1.4E-07	7.22E-11
R-2010	2.74E-03	MMscfh	14,626	12,000	1	0.33					0.068 lb		0.9	0.00	see below <sup>2</sup>	1.8	0.00	1.9	lb/MMscf	0.0	0.00	7.6	lb/MMsc	f 0.1	0.00	0.37	lb/MMBtu	4.9	0.00	5.0E-04	lb/MMscf	6.5E-06	3.27E-09		lb/MMscf	00		1.20E-05 lb			7.85E-11
R-2011	2.74E-03	MMscfh	14,626	12,000	1	0.33					0.068 lb		0.9	0.00	see below2	1.8	0.00	1.9	lb/MMscf	0.0	0.00	7.6	lb/MMsc	f 0.1	0.00	0.37	lb/MMBtu	4.9	0.00	5.0E-04	lb/MMscf	6.5E-06	3.27E-09	1.84E-04		2.4E-06		1.20E-05 lb		1.6E-07	7.85E-11
R-2107	2.26E-03	MMscfh	12,338	11,000	1	0.33					0.068 lb		0.6	0.00	see below <sup>2</sup>	1.4	0.00	1.9	lb/MMscf	0.0	0.00	7.6	lb/MMsc	f 0.1	0.00	0.37	lb/MMBtu	3.4	0.00	5.0E-04	lb/MMscf	4.5E-06	2.27E-09		lb/MMscf	1.7E-06	8.35E-10	1.20E-05 lb	/MMscf	1.1E-07	5.46E-11
R-2108	2.26E-03	MMscfh	12,338	11,000	1	0.33					0.068 lb		0.6	0.00	see below <sup>2</sup>	1.4	0.00	1.9	lb/MMscf	0.0	0.00	7.6	lb/MMsc	f 0.1	0.00	0.37	lb/MMBtu	3.4	0.00	5.0E-04	lb/MMscf	4.5E-06	2.27E-09		lb/MMscf	1.7E-06		1.20E-05 lb		1.1E-07	5.46E-11
R-2069	2.72E-03	MMscfh	9,880	7,000	1	0.33					0.068 lb		0.6	0.00	see below <sup>2</sup>	1.1	0.00	1.9	lb/MMscf	0.0	0.00	7.6	lb/MMsc	f 0.1	0.00	0.37	lb/MMBtu	3.3	0.00	5.0E-04	,	4.4E-06		1.84E-04	lb/MMscf	1.6E-06	8.05E-10	1.20E-05 lb	/MMscf	1.1E-07	5.26E-11
R-2054	2.72E-03	MMscfh	9,880	7,000	1	0.33					0.068 lb		0.6	0.00	see below <sup>2</sup>	1.1	0.00	1.9	lb/MMscf	0.0	0.00	7.6	lb/MMsc	f 0.1	0.00	0.37	lb/MMBtu	3.3	0.00	5.0E-04	lb/MMscf	4.4E-06	2.19E-09	1.84E-04		1.6E-06	8.05E-10	1.20E-05 lb	/MMscf	1.1E-07	5.26E-11
R-2055	4.09E-03	MMscfh	9,880	7,000	1	0.33					0.068 lb	/MMBtu	0.9	0.00	see below <sup>2</sup>	1.6	0.00	1.9	lb/MMscf	0.0	0.00	7.6	lb/MMsc	f 0.1	0.00	0.37	lb/MMBtu	5.0	0.00	5.0E-04	lb/MMscf	6.6E-06	3.30E-09	1.84E-04	lb/MMscf	2.4E-06	1.21E-09	1.20E-05 lb	/MMscf	1.6E-07	7.91E-11
R-2004	2.76E-03	MMscfh	9,880	7,000	1	0.33					0.068 lb	/MMBtu	0.6	0.00	see below <sup>2</sup>	1.1	0.00	1.9	lb/MMscf	0.0	0.00	7.6	lb/MMsc	f 0.1	0.00	0.37	lb/MMBtu	3.4	0.00	5.0E-04	lb/MMscf	4.4E-06	2.22E-09	1.84E-04	lb/MMscf	1.6E-06		1.20E-05 lb		1.1E-07	5.34E-11
R-2007	1.47E-03	MMscfh	14,626	12,000	1	0.33					0.068 lb	/MMBtu	0.5	0.00	see below <sup>2</sup>	1.0	0.00	1.9	lb/MMscf	0.0	0.00	7.6	lb/MMsc	f 0.1	0.00	0.37	lb/MMBtu	2.7	0.00	5.0E-04	lb/MMscf	3.5E-06	1.76E-09	1.84E-04	lb/MMscf	1.3E-06	6.46E-10	1.20E-05 lb	/MMscf	8.4E-08	4.22E-11
R-2020	2.65E-03	MMscfh	9,880	7,000	1	0.33					0.068 lb	/MMBtu	0.6	0.00	see below <sup>2</sup>	1.0	0.00	1.9	lb/MMscf	0.0	0.00	7.6	lb/MMsc	f 0.1	0.00	0.37	lb/MMBtu	3.2	0.00	5.0E-04	lb/MMscf	4.3E-06	2.14E-09	1.84E-04	lb/MMscf	1.6E-06	7.86E-10	1.20E-05 lb	/MMscf	1.0E-07	5.13E-11
R-2053	1.18E-03	MMscfh	14,626	12,000	1	0.33					0.068 lb	/MMBtu	0.4	0.00	see below <sup>2</sup>	0.8	0.00	1.9	lb/MMscf	0.0	0.00	7.6	lb/MMsc	f 0.0	0.00	0.37	lb/MMBtu	2.1	0.00	5.0E-04	lb/MMscf	2.8E-06	1.40E-09	1.84E-04	lb/MMscf	1.0E-06	5.16E-10	1.20E-05 lb	/MMscf	6.7E-08	3.37E-11
R-2070	3.48E-02	MMscfh	12,338	11,000	1	0.33					0.068 lb		9.7	0.00	see below2	21.2	0.01	1.9	lb/MMscf	0.3	0.00	7.6	lb/MMsc	f 1.1	0.00	0.37	lb/MMBtu	52.9	0.03	5.0E-04	lb/MMscf	7.0E-05	3.50E-08	1.84E-04	lb/MMscf	2.6E-05		1.20E-05 lb		1.7E-06	
R-2101	3.57E-02	MMscfh	9,880	7,000	1	0.33					0.068 lb	/MMBtu	8.0	0.00	see below2	13.8	0.01	1.9	lb/MMscf	0.2	0.00	7.6	lb/MMsc	f 0.9	0.00	0.37	lb/MMBtu	43.5	0.02	5.0E-04	lb/MMscf	5.8E-05	2.88E-08	1.84E-04	lb/MMscf	2.1E-05	1.06E-08	1.20E-05 lb	/MMscf	1.4E-06	6.92E-10
R-1023	3.98E-02	MMscfh	9,880	7,000	1	0.33					0.068 lb	/MMBtu	8.9	0.00	see below <sup>2</sup>	15.4	0.01	1.9	lb/MMscf	0.2	0.00	7.6	lb/MMsc	f 1.0	0.00	0.37	lb/MMBtu	48.5	0.02	5.0E-04	lb/MMscf	6.4E-05	3.22E-08	1.84E-04	lb/MMscf	2.4E-05	1.18E-08	1.20E-05 lb	/MMscf	1.5E-06	7.72E-10
R-0920	1.33E-02	MMscfh	14,626	12,000	1	0.33					0.068 lb	/MMBtu	4.4	0.00	see below2	8.9	0.00	1.9	lb/MMscf	0.1	0.00	7.6	lb/MMsc	f 0.5	0.00	0.37	lb/MMBtu	24.1	0.01	5.0E-04	lb/MMscf	3.2E-05	1.59E-08	1.84E-04	lb/MMscf	1.2E-05	5.85E-09	1.20E-05 lb	/MMscf	7.7E-07	3.83E-10
R-2092	2.66E-02	MMscfh	9,880	7,000	1	0.33					0.068 lb	/MMBtu	6.0	0.00	see below <sup>2</sup>	10.3	0.01	1.9	lb/MMscf	0.2	0.00	7.6	lb/MMsc	f 0.7	0.00	0.37	lb/MMBtu	32.5	0.02	5.0E-04	lb/MMscf	4.3E-05	2.15E-08	1.84E-04	lb/MMscf	1.6E-05	7.90E-09	1.20E-05 lb	/MMscf	1.0E-06	5.16E-10
R-0926	2.05E-03	MMscfh	9,880	7,000	1	0.33					0.068 lb	/MMBtu	0.5	0.00	see below2	0.8	0.00	1.9	lb/MMscf	0.0	0.00	7.6	lb/MMsc	f 0.1	0.00	0.37	lb/MMBtu	2.5	0.00	5.0E-04	lb/MMscf	3.3E-06	1.66E-09	1.84E-04	lb/MMscf	1.2E-06	6.08E-10	1.20E-05 lb	/MMscf	8.0E-08	3.98E-11
R-0928	2.05E-03	MMscfh	9,880	7,000	1	0.33					0.068 lb	/MMBtu	0.5	0.00	see below2	0.8	0.00	1.9	lb/MMscf	0.0	0.00	7.6	lb/MMsc	f 0.1	0.00	0.37	lb/MMBtu	2.5	0.00	5.0E-04	lb/MMscf	3.3E-06	1.66E-09	1.84E-04	lb/MMscf	1.2E-06	6.08E-10	1.20E-05 lb	/MMscf	8.0E-08	3.98E-11

	VOC <sup>3</sup>	NO <sub>X</sub>	SO <sub>2</sub>	PM	PM <sub>10</sub> /PM <sub>2.5</sub>	СО	Pb	Hg	Be
Total Projected Actual Emissions		0.0	2 0.05	6.8E-04	1	2.7E-03 0.1		1.8E-07 6.6E-0	08 4.3E-09
Major New Source Review Thresholds		40 40	40	25		15 100		0.6 0.1	0.1
Major New Source Review Triggered?		No No	No	No		No No		No No	No

<sup>1</sup> Event emission rate represents one worst case emergency/malfunction scenario event. Annual emission rate represents the estimated annual average total duration of worst case emergency/malfunction events. <sup>2</sup>SO<sub>2</sub> Emissions Calculation:

SO2 MW (lb/lb-mole)=

SO2 emissions are calculated based on the concentration of sulfur in the gas stream, the ideal gas law, and the molecular weight of SO2.

ar / toodiii.ptii	nio ocou iii ou	.ouidionio					
Variable	Value	Units					
V	1,000,000	ft^3					
P	14.7	psia					
R	10.73	psia-ft^3/lbmol-f					
Т	527.7	R					
md	2596.15	lbmols/MMscf					
	385.1851	scf/lbmol					

Ideal Gas Law used to determine the moles of gas per MSCF (P\*V=n\*R\*T)

Other Notes:

Other Notes:

- Natural gas Higher Heating Value (Btu/sct) = 1020

- The FCU 600 WARP project ties existing blowdown RVs to the FCU Flare header system and consists of emergency RVs only. Nitrogen will be used as the purge gas for the new header tie-ins.

- No modifications to the flare, flare knockout drum, or piping from the knockout drum to the flare required modifications to accommodate the worst case emergency relief scenarios when considering the worst case relief scenarios for the current operations.

- Regulatory applicability for 40 CFR 63, Subpart CC will not change as a result of the project. Emergency RVs are not miscellaneous process vents per 40 CFR 63, Subpart CC since they are exempted from the definition in 40 CFR 63.641

- RV release gas combustion emission factors for PM/PM10/PM2.5, Lead, Beryllium, and Mercury are from AP-42 Section 1.4 (July 1998). Emission factors for VOC, NOx, and CO are from AP-42 Section 13.5 (September 1991). The emissions for SO2 are calculated

Note that VOC emissions will actually decrease with respect to the current scenario where releases are not vented to the Flare; therefore, the potential VOC emissions associated with emergencies and malfunctions will decrease. Refer to the application text for more information.

# **Fugitive Emission Calculations for FCU600 TAR**

LDAR Program: Monitoring per Consent Decree<sup>1</sup>;

Factor Type: Refinery (SDA Factor)

Refinery Screening (EPA Emission Factors EPA-453/R-95-017, Table 2-6)

Annual Hours of Service: 8760

0	Estimated Component	EPA 'Refinery Screening' Factors LEAK	EPA 'Refinery Screening' Factors NO LEAK	Percent	Maximum Uncontrolled Emission Rate	LD&R Control	Percent in VOC	Total VOC Emissions
Component Type	Count	(lb/hr/component)	(lb/hr/component)	Leak	(lbs/hr)	Efficiency <sup>2</sup>	Service	(Tons/yr)
Valves								
Gas/Vapor	10	0.5789	0.0013	2.0%	0.1285	95%	100%	0.03
Light Liquid	26	0.1878	0.0037	2.0%	0.1919	95%	100%	0.04
Heavy Liquid	24	0.00051	0.00051	2.0%	0.0122	30%	100%	0.04
Pumps								
Light Liquid	0	0.9630	0.0265	2.0%	0.0000	80%	100%	0.00
Heavy Liquid	0	0.8565	0.02976	2.0%	0.0000	30%	100%	0.00
Flanges								
Gas/Vapor	26	0.0827	0.00013	0.3%	0.0098	30%	100%	0.03
Light Liquid	78	0.0827	0.00013	0.3%	0.0295	30%	100%	0.09
Heavy Liquid	63	0.0827	0.00013	0.3%	0.0238	30%	100%	0.07
Compressors	0	3.545	0.1971	2.0%	0.0000	0%	100%	0.00
Relief Valves	0	3.728	0.0985	2.0%	0.0000	100%	100%	0.00
Open-ended Lines	0	0.02635	0.0033	2.0%	0.0000	0%	100%	0.00
Sampling Connections	0	0.0827	0.00013	2.0%	0.0000	0%	100%	0.00
					T	otal VOC Emissic	ns (tons/yr):	0.30

<sup>&</sup>lt;sup>1</sup> United States, et.al v. BP Exploration & Oil, et.al., Northern District of Indiana, Hammond Division, Civil Action No. 2:96 CV 095 RL

 $AVO\ monitoring\ equivalent\ to\ 30\%\ control\ is\ applied\ to\ all\ flanges\ and\ heavy\ liquid\ valves\ and\ pumps.$ 

 $30\%\ control\ estimate\ per\ TCEQ\ Guidance\ "Air\ Permit\ Technical\ Guidance\ for\ Chemical\ Sources:\ Equipment\ Leak\ Fugitives"\ (October\ 2000).$ 

Relief Valves are controlled

<sup>&</sup>lt;sup>2</sup> LD&R control efficiency for pumps and valves in gas and light liquid service are 95% and 80%, respectively based on a 500 ppmv leak definition for valves and 2000 ppmv compared to the 10,000 leak definition basis for screening factors (i.e., (1-500/10,000 = 95%) and (1-2,000/10,000) = 80%)

# Fugitive Emission Calculations for WARP at VRU 100

LDAR Program: Monitoring per Consent Decree<sup>1</sup>;

Factor Type: Refinery

Refinery
Screening
(EPA Emission Factors EPA-453/R-95-017, Table 2-6)

Annual Hours of Service: 8760

Component Type	Estimated Component Count	EPA 'Refinery Screening' Factors LEAK (Ib/hr/component)	EPA 'Refinery Screening' Factors NO LEAK (lb/hr/component)	Percent Leak	Maximum Uncontrolled Emission Rate (lbs/hr)	LD&R Control Efficiency <sup>2</sup>	Percent in VOC Service	Total VOC Emissions (Tons/yr)					
Valves													
Gas/Vapor	1	0.5789	0.0013	2.0%	0.0129	95%	100%	0.00					
Light Liquid	15	0.1878	0.0037	2.0%	0.1107	95%	100%	0.02					
Heavy Liquid	0	0.00051	0.00051	2.0%	0.0000	30%	100%	0.00					
Pumps													
Light Liquid	0	0.9630	0.0265	2.0%	0.0000	80%	100%	0.00					
Heavy Liquid	0	0.8565	0.02976	2.0%	0.0000	30%	100%	0.00					
Flanges													
Gas/Vapor	11	0.0827	0.00013	0.3%	0.0042	30%	100%	0.01					
Light Liquid	30	0.0827	0.00013	0.3%	0.0113	30%	100%	0.03					
Heavy Liquid	0	0.0827	0.00013	0.3%	0.0000	30%	100%	0.00					
Compressors	0	3.545	0.1971	2.0%	0.0000	0%	100%	0.00					
Relief Valves - Added <sup>3</sup>	0	3.728	0.0985	2.0%	0.0000	98%	100%	0.00					
Open-ended Lines	0	0.02635	0.0033	2.0%	0.0000	0%	100%	0.00					
Sampling Connections         0         0.0827         0.00013         2.0%         0.0000         0%         100%         0.0													
			Total VC	C Emission	ns Associated with	Added Componer	nts (tons/yr):	0.07					

Valves									
	Gas/Vapor	0	0.5789	0.0013	2.0%	0.0000	95%	100%	0.00
	Light Liquid	-5	0.1878	0.0037	2.0%	-0.0369	95%	100%	-0.01
	Heavy Liquid	0	0.00051	0.00051	2.0%	0.0000	30%	100%	0.00
Flanges									
	Gas/Vapor	0	0.0827	0.00013	0.3%	0.0000	30%	100%	0.00
	Light Liquid	-16	0.0827	0.00013	0.3%	-0.0060	30%	100%	-0.02
	Heavy Liquid	0	0.0827	0.00013	0.3%	0.0000	30%	100%	0.00
				Total VOC	Fmissions	Associated with Re	moved Compone	nts (tons/vr)	-0.03

Past Emissions from Relief Valves -								
Existing Controlled <sup>3</sup>	2	3.728	0.0985	2.0%	0.3422	90%	100%	0.15
Relief Valves - Existing Controlled <sup>3</sup>	2	3.728	0.0985	2.0%	0.3422	98%	100%	0.03
Emissions Reduction (Future - Past)								-0.12
Total VOC Emissions Associated with	Added Compo	nents and Additional C	ontrols (tons/yr):					-0.07

<sup>&</sup>lt;sup>1</sup> United States, et.al v. BP Exploration & Oil, et.al., Northern District of Indiana, Hammond Division, Civil Action No. 2:96 CV 095 RL

<sup>&</sup>lt;sup>2</sup> LD&R control efficiency for pumps and valves in gas and light liquid service are 95% and 80%, respectively based on a 500 ppmv leak definition for valves and 2000 ppmv compared to the 10,000 leak definition basis for screening factors (i.e., (1-500/10,000 = 95%) and (1-2,000/10,000) = 80%)

 $<sup>\</sup>label{eq:avolution} \mbox{AVO monitoring equivalent to 30\% control is applied to all flanges and heavy liquid valves and pumps.}$ 

<sup>30%</sup> control estimate per TCEQ Guidance "Air Permit Technical Guidance for Chemical Sources: Equipment Leak Fugitives" (October 2000).

<sup>&</sup>lt;sup>3</sup> There are no new relief valves and 2existing RV's - previously routed to the atmosphere (through the blowdown stack) that are now routed to the VRU flare. The existing RVs were previously controlled with a water spray chamber that is presumed to be capable of 90% control.

# Fugitive Emission Calculations for WARP at VRU 200

LDAR Program: Monitoring per Consent Decree<sup>1</sup>;

Factor Type: Refinery

Refinery
Screening
(EPA Emission Factors EPA-453/R-95-017, Table 2-6)

Annual Hours of Service: 8760

Component Type	Estimated Component Count	EPA 'Refinery Screening' Factors LEAK (lb/hr/component)	EPA 'Refinery Screening' Factors NO LEAK (lb/hr/component)	Percent Leak	Maximum Uncontrolled Emission Rate (lbs/hr)	LD&R Control Efficiency <sup>2</sup>	Percent in VOC Service	Total VOC Emissions (Tons/yr)
Valves		, , ,			, ,			
Gas/Vapor	1	0.5789	0.0013	2.0%	0.0129	95%	100%	0.00
Light Liquid	3	0.1878	0.0037	2.0%	0.0221	95%	100%	0.00
Heavy Liquid	0	0.00051	0.00051	2.0%	0.0000	30%	100%	0.00
Pumps								
Light Liquid	0	0.9630	0.0265	2.0%	0.0000	80%	100%	0.00
Heavy Liquid	0	0.8565	0.02976	2.0%	0.0000	30%	100%	0.00
Flanges								
Gas/Vapor	7	0.0827	0.00013	0.3%	0.0026	30%	100%	0.01
Light Liquid	7	0.0827	0.00013	0.3%	0.0026	30%	100%	0.01
Heavy Liquid	1	0.0827	0.00013	0.3%	0.0004	30%	100%	0.00
Compressors	0	3.545	0.1971	2.0%	0.0000	0%	100%	0.00
Relief Valves - Added <sup>3</sup>	0	3.728	0.0985	2.0%	0.0000	98%	100%	0.00
Open-ended Lines	0	0.02635	0.0033	2.0%	0.0000	0%	100%	0.00
Sampling Connections	0	0.0827	0.00013	2.0%	0.0000	0%	100%	0.00
			Total VC	C Emission	ns Associated with	Added Componer	nts (tons/yr):	0.03

Valves								
Gas/Vapor	0	0.5789	0.0013	2.0%	0.0000	95%	100%	0.00
Light Liquid	-3	0.1878	0.0037	2.0%	-0.0221	95%	100%	0.00
Heavy Liquid	0	0.00051	0.00051	2.0%	0.0000	30%	100%	0.00
Flanges								
Gas/Vapor	0	0.0827	0.00013	0.3%	0.0000	30%	100%	0.00
Light Liquid	-5	0.0827	0.00013	0.3%	-0.0019	30%	100%	-0.01
Heavy Liquid	0	0.0827	0.00013	0.3%	0.0000	30%	100%	0.00
			Total VOC	Emiccione	Associated with Por	mayad Campana	nte (tone/ur):	-0.01

Past Emissions from Relief Valves -								
Existing Controlled <sup>3</sup>	4	3.728	0.0985	2.0%	0.6844	90%	100%	0.30
Relief Valves - Existing Controlled <sup>3</sup>	4	3.728	0.0985	2.0%	0.6844	98%	100%	0.06
Emissions Reduction (Future - Past)								-0.24
Total VOC Emissions Associated with	Added Compo	nents and Additional C	Controls (tons/vr):					-0.23

<sup>&</sup>lt;sup>1</sup> United States, et.al v. BP Exploration & Oil, et.al., Northern District of Indiana, Hammond Division, Civil Action No. 2:96 CV 095 RL

<sup>&</sup>lt;sup>2</sup> LD&R control efficiency for pumps and valves in gas and light liquid service are 95% and 80%, respectively based on a 500 ppmv leak definition for valves and 2000 ppmv compared to the 10,000 leak definition basis for screening factors (i.e., (1-500/10,000 = 95%) and (1-2,000/10,000) = 80%)

 $<sup>\</sup>label{eq:avolution} \mbox{AVO monitoring equivalent to 30\% control is applied to all flanges and heavy liquid valves and pumps.}$ 

<sup>30%</sup> control estimate per TCEQ Guidance "Air Permit Technical Guidance for Chemical Sources: Equipment Leak Fugitives" (October 2000).

<sup>&</sup>lt;sup>3</sup> There are no new relief valves and 4 existing RV's - previously routed to the atmosphere (through the blowdown stack) that are now routed to the VRU flare. The existing RVs were previously controlled with a water spray chamber that is presumed to be capable of 90% control.

# Increased Sewer Emissions from VRU 100/200 WARP Project due to Added Equipment

# **EQUIPMENT TYPE**

VRU 100/200 - Estimated Counts

Atmospheric Drain Hub	1
Catch Basin (Pad or Paving Drain)	0
Inspection Points	0
Cleanouts	0
Above Ground Sewer Pump Out Points	
Sum of Drains	1
Manhole/Junction Box w/o Vent	
Manhole/Junction Box w/ CC and/or Vent	
OSBL Manholes Per Unit - Sealed	
Flare / Degassing/ KO Tanks (ie Above Ground Junction Boxes)	0
Sealed cover sumps - Gas Traps or other sumps	
Total Manholes/Junction Boxes/Sealed Sumps	0
Below Grade Oily Water Separator - Fixed Roof	
Below Grade Oily Water Separator - Floating Roof	
OSBL Sumps/OWS Per Unit	
Total In ground OWS/Sumps	0
Tanks DGO / LGO / Sour Water service	
Above Ground Oil Water Separator Tanks	
Total Above Ground Tanks	0
Accumptions	

Does Not include Above ground pump out lines as are typically fugitive emissions included with fugitives

Assumptions:

All units will meet Benzene Neshaps Compliance Standards
No COV's will be utilized

					Total
			Em	ission Factor	Emissions
		Units of			
AP-42 Factors - Section 5-1 Petroleum Refining 1/95 - Calculations assume 50% control or		1000 liters			
drains versus uncontrolled drain emissions in AP-42	No. of Units	of flow	Value	Units	(kg/hr)
EMISSION INCREASES					
Drains Controlled	1		0.3	kg/day/unit	0.01
Junction Boxes/Manholes Controlled (Carbon Canister to comply with BWON)	0		0.03	kg/day/unit	0.00
Sealed Manholes	0		0.16	kg/day/unit	0.00
Oil Water Separator and Auxillaries					
OWS	0		0.024	kg/1000 liters flow	0.000
Slop oil tanks/OW surge tanks				Use Tanks Program	0.00
OWS Abv Gr (API) Controlled	0		0.024	kg/1000 liters flow	0.000
Subtotal for Emission Increases					0.01
EMICCION DEODE ACEC					
EMISSION DECREASES			0.0	1 . / 1 / 2	0.00
Area Drains Controlled			0.3	kg/day/unit	0.00
Area Drains Uncontrolled			0.7	kg/day/unit	0.00
Process Drains Controlled			0.3	kg/day/unit	0.00
Process Drains Uncontrolled			0.7	kg/day/unit	0.00
Catch Basins Controlled			0.3	kg/day/unit	0.00
Catch Basins Uncontrolled			0.7	kg/day/unit	0.00
Junction Boxes/Manholes Controlled (Carbon Canister to comply with BWON)			0.03	kg/day/unit	0.00
Sealed Manholes			0.16	kg/day/unit	0.00
Junction Boxes/Manholes Uncontrolled			0.7	kg/day/unit	0.00
Oil Water Separator and Auxillaries					
OWS (API) Controlled			0.024	kg/1000 liters	0.00
OWS (API) Uncontrolled			0.6	kg/1000 liters	0.00
Slop oil tanks/OW surge tanks					0.00
OWS Abv Gr (API) UnControlled			0.024	kg/1000 liters	0.00
OWS Abv Gr (API) Controlled			0.6	kg/1000 liters	0.00
Subtotal for Emission Decreases					0.00
NET EMISSIONS				l/a/br	0.01
INET EINIPOIONS				kg/hr lb/d	
					0.76 278
				lb/yr	
				TPY	0.1

#### Notes:

Notes.			
Emission Source		Units	Source*
			AP-42 (e.g.
Uncontrolled Drain	0.69230769	Kg/day	450/650)
Controlled Drain (with water trap - 50% control of AP-			
42)	0.0145	Kg/hr	BIDa
Sealed Manway Cover (gasketed – 77% of AP-42)	0.022	Kg/hr	BIDb
Uncontrolled Junction Box (same as an Uncontrolled			AP-42 (ref.
Drain)	0.029	Kg/hr	BIDa)
Controlled Junction Box (with carbon canister to			
comply with BWON – 5% of AP-42)	0.00145	Kg/hr	BIDa, BWON
		Kg/1000	
Uncontrolled OWS	0.6	liters	AP-42
		Kg/1000	
Controlled OWS	0.024	liters	AP-42

\*Notes:

BIDa - Background Information Document to Proposed NSPS QQQ, Feb. 1985.

BIDb - Background Information Document to Proposed NSPS QQQ, Dec. 1987.

AP-42 - AP 42, Fifth Edition, Volume I Chapter 5.1 Petroleum Refining, Jan. 1995.

Process			HHV	Sulfur F	Frequency	Duration			VOC				NO <sub>2</sub>	ĸ			SO	)2				PM			PM	10/PM <sub>2.5</sub>				CO				Pb				Hg				Be	
Unit	Malfunction Ra	es B	TU/scf	ppm	#/year	hours	EF	Unit	lb/event	t tpy	EF	U	nit I	lb/event1	tpy	EF	Unit	lb/event1	tpy	EF	Unit	lb/event1	tpy	EF	Unit	lb/event1	tpy	EF	Unit	lb/event1	tpy	EF	Unit	lb/event	tpy	EF	Unit	lb/day	tpy	EF	Unit	lb/day	tpy
SV-963	0.00326 MMs	cfh 1	2,338	11,000	1.0	0.33					0.06	8 lb/M	MBtu	0.9	0.00	see belo	w <sup>2</sup>	2.0	0.00	1.9	lb/MMscf	0.02	0.00	7.6	lb/MMscf	0.10	0.00	0.37	lb/MMBtu	5.0	0.00	5.0E-0	04 lb/MMsc	f 6.6E-06	3.29E-	09 1.84E-	04 lb/MMs	cf 2.4E-0	ô 1.21E-0'	9 1.20E	E-05 lb/MMsc	f 1.6E-0	7.89E-11
SV-972	0.00660 MMs	cfh 9	9,880	7,000	1.0	0.33					0.06	8 lb/M	MBtu	1.5	0.00	see belo	w <sup>2</sup>	2.6	0.00	1.9	lb/MMscf	0.04	0.00	7.6	lb/MMscf	0.16	0.00	0.37	lb/MMBtu	8.0	0.00	5.0E-0	04 lb/MMsc	f 1.1E-05	5.33E-	09 1.84E-	04 lb/MMs	cf 3.9E-0	ô 1.96E-0'	9 1.20E	E-05 lb/MMsc	of 2.6E-0	/ 1.28E-10
T-519	0.01424 MMs	cfh 9	9,880	7,000	1.0	0.33					0.06	8 lb/M	MBtu	3.2	0.00	see belo	w <sup>2</sup>	5.5	0.00	1.9	lb/MMscf	0.09	0.00	7.6	lb/MMscf	0.35	0.00	0.37	lb/MMBtu	17.3	0.01	5.0E-0	04 lb/MMsc	f 2.3E-05	1.15E-	08 1.84E-	04 lb/MMs	cf 8.4E-0	ô 4.22E-0'	9 1.20E	E-05 lb/MMsc	of 5.5E-0	7 2.76E-10
T-528	0.00467 MMs	cfh 9	9,880	7,000	1.0	0.33					0.06	8 lb/M	MBtu	1.0	0.00	see belo	w <sup>2</sup>	1.8	0.00	1.9	lb/MMscf	0.03	0.00	7.6	lb/MMscf	0.11	0.00	0.37	lb/MMBtu	5.7	0.00	5.0E-0	04 lb/MMsc	f 7.5E-06	3.77E-	09 1.84E-	04 lb/MMs	cf 2.8E-0	ô 1.38E-0'	9 1.20E	E-05 lb/MMsc	f 1.8E-0	7 9.05E-11
T-526	0.00242 MMs	cfh 1	2,338	11,000	1.0	0.33					0.06	8 lb/M	MBtu	0.7	0.00	see belo	w²	1.5	0.00	1.9	lb/MMscf	0.02	0.00	7.6	lb/MMscf	0.07	0.00	0.37	lb/MMBtu	3.7	0.00	5.0E-0	04 lb/MMsc	f 4.9E-06	2.44E-	09 1.84E-	04 lb/MMs	cf 1.8E-0	ô 8.94E-1/	0 1.20E	E-05 lb/MMsc	f 1.2E-0	/ 5.84E-11
T-530	0.00638 MMs	cfh 9	9,880	7,000	1.0	0.33					0.06	8 lb/M	MBtu	1.4	0.00	see belo	w <sup>2</sup>	2.5	0.00	1.9	lb/MMscf	0.04	0.00	7.6	lb/MMscf	0.16	0.00	0.37	lb/MMBtu	7.8	0.00	5.0E-0	04 lb/MMsc	f 1.0E-05	5.15E-	09 1.84E-	04 lb/MMs	cf 3.8E-0	ô 1.89E-0'	9 1.20E	E-05 lb/MMsc	of 2.5E-0	7 1.24E-10

	VOC <sup>3</sup>		NO <sub>X</sub>	SO <sub>2</sub>	PM	PM <sub>10</sub> /PM <sub>2.5</sub>	СО	Pb	Hg	Be
Total Projected Actual Emissions			4.4E-03	0.01	1.2E-04	4.8E-04	0.02	3.1E-08	1.2E-08	7.6E-10
Major New Source Review Thresholds		40	40	40	25	15	100	0.6	0.1	0.1
Major New Source Review Triggered?		No	No	No	No	No	No	No	No	No

<sup>1</sup> Event emission rate represents one worst case emergency/malfunction scenario event. Annual emission rate represents the estimated annual average total duration of worst case emergency/malfunction events.

<sup>2</sup>SO<sub>2</sub> Emissions Calculation:

SO2 MW (lb/lb-mole)=

SO2 emissions are calculated based on the concentration of sulfur in the gas stream, the ideal gas law, and the molecular weight of SO2.

General Assumptions Used in Calculations Value 1,000,000 ft^3 14.7 psia 10.73 psia-ft^3/lbmol-R 527.7 R 2596.15 lbmols/MMscf 385.1851 scf/lbmol

Ideal Gas Law used to determine the moles of gas per MSCF (P\*V=n\*R\*T)

Note that VOC emissions will actually decrease with respect to the current scenario where releases are not vented to the Flare; therefore, the potential VOC emissions associated with emergencies and malfunctions will decrease. Refer to the application text for more information.

- Other Notes:

   Natural gas Higher Heating Value (Btu/scf) = 1020

   The VRU WARP project ties existing blowdown RVs to the VRU Flare header system from VRU 100 and VRU 200 and consists of emergency RVs only. Nitrogen will be used as the purge gas for the new header tie-ins.

   No modifications to the flare, flare knockout drum, or piping from the knockout drum to the flare required modifications to accommodate the worst case emergency relief scenarios when considering the worst case relief scenarios for the current operations.

   Regulatory applicability for 40 CFR 63, Subpart CC will not change as a result of the project. Emergency RVs are not miscellaneous process vents per 40 CFR 63, Subpart CC since they are exempted from the definition in 40 CFR 63.641

   RV release gas combustion emission factors for PM/PM10/PM2.5, Lead, Beryllium and Mercury are from AP-42 Section 1.4 (July 1998). Emission factors for VOC, NOx, and CO are from AP-42 Section 13.5 (September 1991). The emissions for SO2 are calculated It was also conservatively assumed that each RV would lift one time per year, although this is an unlikely scenario.

# **Fugitive Emission Calculations for TK-3637**

LDAR Program: Monitoring per Consent Decree<sup>1</sup>;

Factor Type: Refinery

Screening (EPA Emission

(EPA Emission Factors EPA-453/R-95-017, Table 2-6)

Annual Hours of Service: 8760

Component Type	Estimated Component Count	EPA 'Refinery Screening' Factors LEAK (lb/hr/component)	EPA 'Refinery Screening' Factors NO LEAK (lb/hr/component)	Percent Leak	Maximum Uncontrolled Emission Rate (lbs/hr)	LD&R Control Efficiency <sup>2</sup>	Percent in VOC Service	Total VOC Emissions (Tons/yr)
Valves								
Gas/Vapor	0	0.5789	0.0013	2.0%	0.0000	95%	100%	0.00
Light Liquid	10	0.1878	0.0037	2.0%	0.0738	95%	100%	0.02
Heavy Liquid	0	0.00051	0.00051	2.0%	0.0000	30%	100%	0.00
Pumps								
Light Liquid	0	0.9630	0.0265	2.0%	0.0000	80%	100%	0.00
Heavy Liquid	0	0.8565	0.02976	2.0%	0.0000	30%	100%	0.00
Flanges								
Gas/Vapor	0	0.0827	0.00013	0.3%	0.0000	30%	100%	0.00
Light Liquid	22	0.0827	0.00013	0.3%	0.0083	30%	100%	0.03
Heavy Liquid	0	0.0827	0.00013	0.3%	0.0000	30%	100%	0.00
Compressors	0	3.545	0.1971	2.0%	0.0000	0%	100%	0.00
Relief Valves	0	3.728	0.0985	2.0%	0.0000	100%	100%	0.00
Open-ended Lines	0	0.02635	0.0033	2.0%	0.0000	0%	100%	0.00
Sampling Connections	0	0.0827	0.00013	2.0%	0.0000	0%	100%	0.00
					Т	otal VOC Emission	ons (tons/yr):	0.04

<sup>&</sup>lt;sup>1</sup> United States, et.al v. BP Exploration & Oil, et.al., Northern District of Indiana, Hammond Division, Civil Action No. 2:96 CV 095 RL

 $AVO\ monitoring\ equivalent\ to\ 30\%\ control\ is\ applied\ to\ all\ flanges\ and\ heavy\ liquid\ valves\ and\ pumps.$ 

Relief Valves are controlled

<sup>&</sup>lt;sup>2</sup> LD&R control efficiency for pumps and valves in gas and light liquid service are 95% and 80%, respectively based on a 500 ppmv leak definition for valves and 2000 ppmv compared to the 10,000 leak definition basis for screening factors (i.e., (1-500/10,000 = 95%) and (1-2,000/10,000) = 80%)

 $<sup>30\% \</sup> control\ estimate\ per\ TCEQ\ Guidance\ "Air\ Permit\ Technical\ Guidance\ for\ Chemical\ Sources:\ Equipment\ Leak\ Fugitives"\ (October\ 2000).$ 

3SPS potential emissions are presented below only for reference for determining the particulate emissions from the SCR. The 3SPS boilers will not be modified for this project since the SCR will be an add-on control.

Process Unit	Maximur	m Heat Canacity			VOC			NOx				SC	)2			PM	1			PM10/	PM2.5			С	0			PI	5	
1 locess offin	WIGAIITIGE	II I leat Capacity	EF	Unit	lb/hr	tpy	EF	Unit	lb/hr	tpy	EF	Unit	lb/hr	tpy	EF	Unit	lb/hr	tpy	EF	Unit	lb/hr	tpy	EF	Unit	lb/hr	tpy	EF	Unit	lb/hr	tpy
3SPS	2,774	MMBtu/hour									24.45	lb/MMscf	56.4	246.9																
Fired Heater	198	MMBtu/hour	5.5	lb/MMscf	1.	.1 4.7	0.05	lb/MMBtu	9.89	43.3	26.44	lb/MMscf	4.3	19.0	1.9	lb/MMscf	0.4	1.6	7.6	lb/MMscf	1.5	6.5	0.02	lb/MMBtu	4.0	17.3	5.0E-04	lb/MMscf	9.7E-05	4.2E-04

NOx emissions calculated above are pre-SCR, uncontrolled emissions.

Conversion Rate	3.0%
NOX Reduction (from inlet to SCR)	95%
NSPS J Limit (ppm)	159
TRS Reported in 2005 (ppm)	147
Calculated SO2 Emission Factor at NSPS J Limit (lb/MMscf)	26.44
Calculated SO2 Emission Factor at Current Maximum Average TRS (lb/MMscf)	24.45
Duct Burner ppm sulfur	159.00
Duct Burner SO2 Emission Factor (lb/MMscf)	26.44
Refinery Fuel Gas HHV (BTU/scf)	1203.33
3 SPS Boiler Utilization Factor	0.965

Project Potential to Emit Increase - for permitting level applicability Conversion to Ammonium Sulfate

	Control Device	90 +	o SO <sub>2</sub> Conversion Rate			VUC				NOX				50	)2			PW				PINTU/PI	WIZ.5			C	U			н	D			Sulturic /	ACIO MIST				mercui	, y	/ /		Beryi	4um	
	CONTROL DEVICE	3021	0 303 Conversion Nate	EF	Unit	lb/hr	tpy	EF	U	Init	lb/hr	tpy	EF	Unit	lb/hr	tpy	EF	Unit	lb/hr	tpy	EF	Unit	lb/hr	tpy	EF	Unit	lb/hr	tpy	EF	Unit	lb/hr	tpy	EF	Unit	lb/hr	tpy	EF	F U	nit	lb/hr	tpy	EF	Unit	lb/hr	tpy
	SCR Impact on Boilers	3.0%	% Conversion Rate	n/a	n/a	n/a	n/a	n/a	n	n/a	n/a	n/a	n/a	n/a	n/a	n/a					n/a	n/a	3.5	15.3	n/a	n/a	n/a	n/a	n/a	n/a	n/a	n/a	n/a	n/a	n/a	n/a	n/a	a r	/a	n/a	n/a	n/a	n/a	n/a	n/a
_																																													
	Duct Burners	198	MMBtu/hour			1.	.1 4.	7			9.9	43.3			4.3	19.0	1.9 lb/	MMscf	0.4	1.6			1.7	7.6			4.0	17.3			0.0	0.0				0.9	9 1	1.8E-07 lb/MN	ИBtu	3.6E-05	1.6E-04	1.2E-08	lb/MMBtu	2.3E-06	1.0E-05
			Project PTE				4.	7				43.3				19.0								22.9				17.3								0.9	)				1.6E-04				1.0E-05
		Project PTE (	(with NOx controls included)	1)			4.	7				2.2				19.0								22.9				17.3																	
			Part 70 Minor Part 70 Significant	r			2	.7				4.6				10								5				25																	
			Part 70 Significant	ıt				25				25				25								25				100																	
			Part 70 Permit Required?	?			Ye	es				Yes				Yes								Yes				No																	

Project Emissions Increase - for major NSR applicability

Potential 3SPS Gas Usage Rate (based on maximum heat input capacity and utilization factor)		Po	tential SO2	
MMscf/year	EF	Unit	lb/hr	tpy
20,196.89	24.45	lb/MMscf	n/a	246.9
Potential Duct Burner SO2 Emissions	26.44	lb/MMscf	4.3	19.0
Total Potential SO2 Emissions				265.9

onversion to Ammonium :	Sulfate																																							
Control Device	SO <sub>2</sub> to SO <sub>2</sub> Conversion Rate		VOC				NOx			SO2			PM /			PM10/PM2.5			CO		Pb			Sulfuric Acid Mist			Mercury			Beryllium										
Control Device	302 to 303 Conversion Nate	EF	Unit	lb/hr	tpy	EF	Unit	lb/hr	tpy	EF	Unit	lb/hr	tpy	EF U	nit lb	/hr	tpy E	Unit	lb/hr	tpy	EF	Unit	lb/hr	tpy	EF	Unit	lb/hr	tpy	EF	Unit	lb/hr	tpy	EF	Unit	lb/hr	tpy	EF	Unit	lb/hr	tpy
SCR Impact on Boilers	3.0% % Conversion Rate	n/a	n/a	n/a	n/a	n/a	n/a	n/a	n/a	n/a	n/a	n/a	n/a				n/	a n/a	n/a	15.	.3 n/a	n/a	n/a	n/a	n/a	n/a	n/a	n/a	n/a	n/a	n/a	n/a	n/a	n/a	n/a	n/a	n/a	n/a	n/a	n/a
	•				•	•	•	•	•					•					•	•	•																	•		
Duct Burners	198 MMBtu/hour				4.7				2.2				19.0	1.9 lb/N	Mscf	0.4	1.6			7.	.6			17.3				0.0	n/a r	n/a r	n/a	0.87	1.8E-	-07 lb/MMBtu	3.6E-05	1.6E-04	1.2E-08	lb/MMBtu	2.3E-06	1.0E-05
•	•	•			•	•	•		•					•		•		•		•			•				-	•	•	•								•		
	Project Emissions Increas	9			4.7				2.2				19.0				1.6			22.	.9			17.3				4.2E-04				0.9				1.6E-04				1.0E-05
	Duct Burner and SCR Baseline Emission	5			-				-				-							-								-				-				-	1			-

Assumptions:

- Maximum Heat Input Capacity = 575 MMBturbr \*5 Boilers \*96.5% availability at 3SPS
- Projected actual gas usage rates are based on assuming 8,760 hours of operation at the maximum permitted capacity.
- No cred is currently taken for NOx reductions from the boilers.
- Post \*SCR NOx emissions are based on vendor guarantee emission rates using SCR technology.
- Since the duct burners are new units, PTE is used for the projected actual emissions.
- SiO2 emissions are calculated using Refinery fuel gas HHV before the CXHD project and the Ideal Gas Law
- Fuel Gas Hearting Value = 1203.3 BTU/scf

- Natural Gas Heating Value = 1020 BTU/scf

-Ammonium Sulfate Molecular Weight = 132.14
-Sulfur Trioxide Molecular Weight = 80.06
-Sulfur Dioxide Molecular Weight = 80.06
-Sulfur Dioxide Molecular Weight = 64.06
-Sulfur Dioxide Molecular Weight = 90.00
-Sulfur Can Mist Molecular Weight = 90.00
-Sulfur Can Mist Molecular Weight = 90.00
-BP is conservatively considering that all of the SO<sub>3</sub> enitted can form bot condensable particulate matter and sulfuric acid mist.
-Fraction of SO<sub>3</sub> converted to Sulfuric Acid Mist = 1
-Moles in 1 MMscl (n from Ideal Gas Law) (ibmol/Mmscl) 2596.15 Derived from the Ideal Gas Law, assuming V = 1MMscl, P = 14.7 psia, T = 527.7 R, R = 10.73 psia-fr-3/lbmol-R

# **Fugitive Emission Calculations for New Boilers**

LDAR Program: Monitoring per Consent Decree<sup>1</sup>;

Factor Type: Refinery (EBA Emis

Screening

(EPA Emission Factors EPA-453/R-95-017, Table 2-6)

Annual Hours of Service: 8760

Component Type	Estimated Component Count	EPA 'Refinery Screening' Factors LEAK (lb/hr/component)	EPA 'Refinery Screening' Factors NO LEAK (lb/hr/component)	Percent Leak	Maximum Uncontrolled Emission Rate (lbs/hr)	LD&R Control Efficiency <sup>2</sup>	Percent in VOC Service	Total VOC Emissions (Tons/yr)
Valves								
Gas/Vapor	126	0.5789	0.0013	2.0%	1.6194	95%	100%	0.35
Light Liquid	0	0.1878	0.0037	2.0%	0.0000	95%	100%	0.00
Heavy Liquid	0	0.00051	0.00051	2.0%	0.0000	30%	100%	0.00
Pumps								
Light Liquid	0	0.9630	0.0265	2.0%	0.0000	80%	100%	0.00
Heavy Liquid	0	0.8565	0.02976	2.0%	0.0000	30%	100%	0.00
Flanges								ı
Gas/Vapor	76	0.0827	0.00013	0.3%	0.0287	30%	100%	0.09
Light Liquid	0	0.0827	0.00013	0.3%	0.0000	30%	100%	0.00
Heavy Liquid	0	0.0827	0.00013	0.3%	0.0000	30%	100%	0.00
Compressors	0	3.545	0.1971	2.0%	0.0000	0%	100%	0.00
Relief Valves	3	3.728	0.0985	2.0%	0.5133	100%	100%	0.00
Open-ended Lines	0	0.02635	0.0033	2.0%	0.0000	0%	100%	0.00
Sampling Connections	1	0.0827	0.00013	2.0%	0.0018	0%	100%	0.01
					Т	otal VOC Emission	ons (tons/yr):	0.45

<sup>&</sup>lt;sup>1</sup> United States, et.al v. BP Exploration & Oil, et.al., Northern District of Indiana, Hammond Division, Civil Action No. 2:96 CV 095 RL

 $AVO\ monitoring\ equivalent\ to\ 30\%\ control\ is\ applied\ to\ all\ flanges\ and\ heavy\ liquid\ valves\ and\ pumps.$ 

30% control estimate per TCEQ Guidance "Air Permit Technical Guidance for Chemical Sources: Equipment Leak Fugitives" (October 2000). Relief Valves are controlled

<sup>&</sup>lt;sup>2</sup> LD&R control efficiency for pumps and valves in gas and light liquid service are 95% and 80%, respectively based on a 500 ppmv leak definition for valves and 2000 ppmv compared to the 10,000 leak definition basis for screening factors (i.e., (1-500/10,000 = 95%) and (1-2,000/10,000) = 80%)

# Fugitive Emission Calculations for Fuel Gas Lines for 3 SPS SCR Duct Burners

LDAR Program: Monitoring per Consent Decree<sup>1</sup>;

Factor Type: Refinery (50.5 Section 5.2)

Refinery Screening (EPA Emission Factors EPA-453/R-95-017, Table 2-6)

Annual Hours of Service: 8760

Component Type	Estimated Component Count	EPA 'Refinery Screening' Factors LEAK (lb/hr/component)	EPA 'Refinery Screening' Factors NO LEAK (lb/hr/component)	Percent Leak	Maximum Uncontrolled Emission Rate (lbs/hr)	LD&R Control Efficiency <sup>2</sup>	Percent in VOC Service	Total VOC Emissions (Tons/yr)
Valves								
Gas/Vapor	150	0.5789	0.0013	2.0%	1.9278	95%	100%	0.42
Pumps								
Light Liquid	0	0.9630	0.0265	2.0%	0.0000	80%	100%	0.00
Heavy Liquid	0	0.8565	0.02976	2.0%	0.0000	30%	100%	0.00
Flanges								
Gas/Vapor	255	0.0827	0.00013	0.3%	0.0963	30%	100%	0.30
Light Liquid	0	0.0827	0.00013	0.3%	0.0000	30%	100%	0.00
Heavy Liquid	0	0.0827	0.00013	0.3%	0.0000	30%	100%	0.00
Compressors	0	3.545	0.1971	2.0%	0.0000	0%	100%	0.00
Relief Valves	0	3.728	0.0985	2.0%	0.0000	100%	100%	0.00
Open-ended Lines	10	0.02635	0.0033	2.0%	0.0376	0%	100%	0.16
Sampling Connections	0	0.0827	0.00013	2.0%	0.0000	0%	100%	0.00
					Т	otal VOC Emission	ons (tons/yr):	0.88

<sup>&</sup>lt;sup>1</sup> United States, et.al v. BP Exploration & Oil, et.al., Northern District of Indiana, Hammond Division, Civil Action No. 2:96 CV 095 RL

 $\label{eq:average_average} \text{AVO monitoring equivalent to 30\% control is applied to all flanges and heavy liquid valves and pumps.}$ 

30% control estimate per TCEQ Guidance "Air Permit Technical Guidance for Chemical Sources: Equipment Leak Fugitives" (October 2000).

<sup>&</sup>lt;sup>2</sup> LD&R control efficiency for pumps and valves in gas and light liquid service are 95% and 80%, respectively based on a 500 ppmv leak definition for valves and 2000 ppmv compared to the 10,000 leak definition basis for screening factors (i.e., (1-500//10,000 = 95%) and (1-2,000/10,000) = 80%)

1131 Required Boiler Heat Input (MMBTU/hr)\* (2 boilers at 580 MMBtu/hr each at 97.5% total annual utilization)

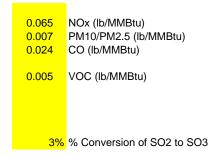
#### **Conservative Emissions Case**

COMOON TOO			
·	Emission		
	Factor**	Emissions	Emissions
Pollutant	(lb/MMBtu)	(lb/hr)	(tpy)
NOx	0.065	73.5	322.0
SO2	***	20.0	49.8
PM	0.002	2.1	9.2
PM10/PM			
2.5	0.007	9.7	40.0
CO	0.024	27.1	118.9
VOC	0.005	6.1	26.7
Sulfuric			
Acid Mist	5.E-04	0.5	2.3
Lead	4.9.E-07	6.E-04	2.E-03
Mercury	1.8E-07	2.E-04	9.E-04
Berylllium	1.18E-08	1.E-05	6.E-05

- \*\* EF Notes:
- 1) NOx factor based on manufacturer's guarantee (control technology/technique to be determined)
- SO2 emissions will be limited to 24.9 tpy per boiler and emissions will be calculated based on total sulfur in refinery fuel gas. Natural gas blending will be used, if necessary.
- 3) PM based on AP-42 Table 1.4-2.
- 4) PM10/PM2.5 emission factor based on AP-42 Table 1.4-2 total particulate (condensible and filterable); Note that additional PM10/PM2.5 emissions were added, assuming that an SCR may be added to the boilers and 3% conversion of SO2 emissions to SO3 and ammonium sulfate.
- 5) CO based on manufacturer's guarantee.
- 6) Refinery fuel gas heating value assumed to be 1200 BTU/scf
- 7) VOC based on AP-42 Section 1.4 for natural gas
- 8) Lead, beryllium, and mercury emissions based on AP-42 Section 1.4 for natural gas.
- 9) Sulfuric Acid Mist emissions based on assumed conversion percentage of SO2 to SO3 and the assumption that all SO3 converts to sulfuric acid mist.

Refinery Fuel Gas HHV (BTU/scf)	1200
Natural Gas HHV (BTU/scf)	1020
Natural Gas SO2 Emission Factor	
(lb/MMscf)	0.6
Refinery Fuel Gas SO2 Emission	
Factor (at S ppm listed above)	
(lb/MMscf)	0.0

8760 Hours of Operation



64.06 Molecular Weight of SO2 98.07 Molecular Weight of H2SO4

#### 3 SPS Baseline for CO Reduction

F-factor 8710 scf/mmbtu 7.27E-08 K-factor for CO 28 CO MW

CO and O2 Analyzer Data:

	%O2		(	CO (ppm)		MMSCF/yr		BTU/scf		MMBTU/yr		lb/MMBTU		CO (tpy)	
_	2004	2005	2004	2005	2004	2005	2004	2005	2004	2005	2004	2005	2004	2005	
Boiler 31	9.36	8.45	27.24	90.9	2690.84	2749.28	1150.09	1279.182	3,094,708	3,516,834	0.031248	0.096657	48.3512	169.9629	
Boiler 32	6.21	9.59	24.85	20.3	3213.87	2408.26	1150.09	1279.182	3,696,238	3,080,596	0.022404	0.023803	41.40467	36.66309	
Boiler 33	5.88	7.46	39.91	30.4	3173.27	2616.82	1150.09	1279.182	3,649,546	3,347,394	0.035174	0.02995	64.18397	50.12744	
Boiler 34	8.96	8.17	15.77	53.5	2748.05	2703.50	1150.09	1279.182	3,160,510	3,458,261	0.017484	0.055669	27.62978	96.25842	
Boiler 36	6.79	7.71	57.16	60.5	3045.04	2718.25	1150.09	1279.182	3,502,070	3,477,131	0.053638	0.060762	93.92229	105.6381	
TOTAL												Т	OTAL 275.4919	458.6499	

boiler	31	32	33	34	36	Total
Averages 2004-2005	109.16	39.03388	57.15571	61.94410002	99.78019	367.07

#### Notes:

- %O2, ppm CO and MMSCF/yr are annual average values obtained from averaging monthly CEMS and analyzer data
   Note that this conservatively uses CO analyzer data instead of the data reported in the TRI/I-Steps based on the emission factor.

Potential to Emit for 3 SPS Boilers Based on Vendor Guaranteed Emission Factor and Limited Utilization Factor of 96.5%

Process	Maximum	Heat Capacity		CO								
Unit	Maximum	пеат Сараспу	EF	Unit	lb/hr	tpy						
3SPS 1	555	MMBtu/hour	0.02	lb/MMBtu	11.1	48.6	per boiler					
3SPS 2	555	MMBtu/hour	0.02	lb/MMBtu	11.1	48.6						
3SPS 3	555	MMBtu/hour	0.02	lb/MMBtu	11.1	48.6						
3SPS 4	555	MMBtu/hour	0.02	lb/MMBtu	11.1	48.6						
3SPS 6	555	MMBtu/hour	0.02	lb/MMBtu	11.1	48.6						

CO Emission Factor is based on vendor guarantee.

#### CO Emissions Reductions from 3 SPS Boilers

Boiler	CO	
	tpy	
1	(60.5)	Future Potential CO Emissions - Past Actual CO Emissions
2	9.6	
3	(8.5)	
4	(13.3)	
6	(51.2)	
Total	(124.0)	Total CO Reduction
		<del>-</del>

### Tank 8

Tank 8 is an oil/water separator that currently handles the wastewater associated with the 11 Pipe Stills. This is a new oil/water separator system that may eventually replace Tank 8; however, both may operate for a period of time.

# Estimated New Fugitive Components Associated with the Tank 8 Oil/Water Separator System

Component Type Valves	# of components
Gas/Vapor	15
Light Liquid	15
Heavy Liquid	50

#### **Pumps**

Light Liquid	
Heavy Liquid	15

### **Flanges**

Gas/Vapor	20
Light Liquid	20
Heavy Liquid	40

Compressors	0
Relief Valves	5
Open-ended Lines	0
Sampling Connections	8

### New Tank 8 Oil/Water Separator System

Maximum average daily		
estimated flow rate of		
material through the new		
Tank 8 oil/water separator		
(gal/day)	100,000	Based on design estimates
VOC Emission Factor		
(lb/kgal)	0.2	Covered Oil/Water Separator from AP-42 Table 5.1-2 (1/95)
VOC Emissions (lbs/day)	20	Maximum average daily flow rate * VOC Emission Factor
VOC Emissions (tpy)	3.7	VOC Emissions lbs/day * 365 days /yr * 1 ton/2,000 lbs

Note that the oil/water separator will be subject to the requirements of 40 CFR 61, Subpart FF and will be equipped with carbon canisters to control emissions.

Note that a new junction box and new manhole and sewer drain may be installed, depending on the final location chosen within the refinery.

# **Fugitive Emission Calculations for Tank 8 OWS Replacement**

LDAR Program: Monitoring per Consent Decree<sup>1</sup>;

Factor Type: Refinery

Refinery Screening (EPA Emission Factors EPA-453/R-95-017, Table 2-6)

Annual Hours of Service: 8760

Component Type	Estimated Component Count	EPA 'Refinery Screening' Factors LEAK (lb/hr/component)	EPA 'Refinery Screening' Factors NO LEAK (lb/hr/component)	Percent Leak	Maximum Uncontrolled Emission Rate (lbs/hr)	LD&R Control Efficiency <sup>2</sup>	Percent in VOC Service	Total VOC Emissions (Tons/yr)
Valves								
Gas/Vapor	15	0.5789	0.0013	2.0%	0.1928	95%	100%	0.04
Light Liquid	15	0.1878	0.0037	2.0%	0.1107	95%	100%	0.02
Heavy Liquid	50	0.00051	0.00051	2.0%	0.0255	30%	100%	0.08
Pumps								
Light Liquid	0	0.9630	0.0265	2.0%	0.0000	80%	100%	0.00
Heavy Liquid	15	0.8565	0.02976	2.0%	0.6944	30%	100%	2.13
Flanges								
Gas/Vapor	20	0.0827	0.00013	0.3%	0.0076	30%	100%	0.02
Light Liquid	20	0.0827	0.00013	0.3%	0.0076	30%	100%	0.02
Heavy Liquid	40	0.0827	0.00013	0.3%	0.0151	30%	100%	0.05
Compressors	0	3.545	0.1971	2.0%	0.0000	0%	100%	0.00
Relief Valves	5	3.728	0.0985	2.0%	0.8555	100%	100%	0.00
Open-ended Lines	0	0.02635	0.0033	2.0%	0.0000	0%	100%	0.00
Sampling Connections	8	0.0827	0.00013	2.0%	0.0143	0%	100%	0.06
	_	_	_	•	Т	otal VOC Emission	ons (tons/yr):	2.43

<sup>&</sup>lt;sup>1</sup> United States, et.al v. BP Exploration & Oil, et.al., Northern District of Indiana, Hammond Division, Civil Action No. 2:96 CV 095 RL

<sup>&</sup>lt;sup>2</sup> LD&R control efficiency for pumps and valves in gas and light liquid service are 95% and 80%, respectively based on a 500 ppmv leak definition for valves and 2000 ppmv compared to the 10,000 leak definition basis for screening factors (i.e., (1-500/10,000 = 95%) and (1-2,000/10,000) = 80%)

 $<sup>\</sup>label{eq:average_average} \text{AVO monitoring equivalent to 30\% control is applied to all flanges and heavy liquid valves and pumps.}$ 

<sup>30%</sup> control estimate per TCEQ Guidance "Air Permit Technical Guidance for Chemical Sources: Equipment Leak Fugitives" (October 2000). Relief Valves are controlled

#### **Diesel Fire Pump Engines Emissions**

There are three identical diesel fire pump engines

Hours of Operation	500 Emergency	fire pump engines used for the fire water system
Number of Engines	3	
Engine HP	390 Actual mech	nanical HP estimated based on the mechanical effciency, assumed 0.9
Load Factor	100% Conservativ	ely assumes that pump engine is operated at 100% load, actual load depends on operating point of engine/pump combination

		NO <sub>x</sub>		СО		PM/PM <sub>10</sub> /PM <sub>2.5</sub>		SO <sub>x</sub>		VOC
		AP-42	NSPS IIII	AP-42	NSPS IIII	AP-42	NSPS IIII	AP-42	Low Sulfur Diesel	AP-42
Emission Factor (lb/hp*hr)		0.031		0.00668		0.0022		0.00205		0.00251
Emission Factor (g/hp*hr)		14.0616	7.8	3.030048	2.6	0.99792	0.4	0.92988	0.161	1.138536
Emission Factor (g/kw*hr)		18.848	10.5	4.06144	3.5	1.3376	0.54	1.2464		1.52608
Emissions (lb/hr)	each engine	6.	71	2.	24	0.	34	0.	14	0.98
Emissions (tpy)	each engine	1.	68	0.	56	0.	09	0.	03	0.24
Total Emissions (lb/hr)		20	.12	6.	71	1.	03	0.	42	2.94
Total Emissions (tpy)		5.	03	1.	68	0.	26	0.	10	0.73

#### Notes

Emission factors are from AP-42 Section 3.3, Table 3.3-1 (10/96) and NSPS Subpart IIII.

VOC emission factor is the sum of the TOC emission factors for exhaust and crankcase.

PM is assumed to be equal to PM<sub>10</sub> for the purposes of these calculations. It should be noted that AP-42 Section 3.3 does not include a PM emission factor, and footnote b of Table 3.3-1 indicates that all particulate is assumed to be less than 1 micrometer.

Emission factors noted in red are emission standards for engine 300~600 HP, per 40 CFR 60, Subpart IIII

Emission estimates are based on the lower of AP-42 emission factors and Subpart IIII emission limits

40 CFR Subpart IIII limits NOx + NMHC. NOx assumed emitted at Subpart IIII limit and VOC emitted at AP-42 factor levels.

SO2 emission factor based on NSPS limit of 500 ppm fuel sulfur content and calculations below.

#### Sample Calculation

NOx emissions from compressor (lb/hr) =	390 hp	7.8 g NOx	lb	100%	3 engines = 20.12 lb NOx	/hr	
, ,		hp-hr	453.6 g		<u> </u>		
SO2 emission factor							
calculation:	0.0005 lb S	7.1 lb diesel	gal diesel	2 lb SO2	7000 MMBtu	453.6 g	0.161g SO2/hp-hr
	lb diesel	gal diesel	.140 MMBtu	lb S	10^6 hp-hr	lb	_

Conversion factors found in AP-42 Table 3.3-1 were used above to calculate engine fuel efficiency in MMBtu/hp-hr

# Summary of Dewatering and Thermal Desorption System Project Emission Calculations

	VOC	NOx	PM	PM10/PM2.5	CO	SO2
	(tons/yr)	(tons/yr)	(tons/yr)	(tons/yr)	(tons/yr)	(tons/yr)
Dewatering Emissions	0.9	n/a	n/a	n/a	n/a	n/a
Thermal Desorption Emissions (Burners and VOC)	1.0	5.2	0.5	8.0	1.3	1.8
Fugitive Equipment Components	0.6	n/a	n/a	n/a	n/a	n/a
TOTAL	2.4	5.2	0.5	0.8	1.3	1.8
PERMITTING STATUS	EXEMPT	PERMIT REQUIRED	EXEMPT	EXEMPT	EXEMPT	EXEMPT
Permitting Thresholds:						
Part 70 Minor Source Mod	2.7	4.6	5	5	25	10
Part 70 Significant Source Mod	25	25	25	25	100	25

Refer to the application text for a description of the dewatering system.

#### **Mass Balance Emissions Calculation**

Maximum values from sludge analytical data from 2000 to 2002 documented in Hazardous Waste Combustor MACT Performance Test Plans

DAF Float/Biosolids | API Sludge |

_		DAF Float/Biosolids	API Sluage
Method 8270 (SVOCs)		mg/kg	mg/kg
Anthracene		9.9	ND
Chyrsene		16.5	ND
Naphthalene		149	47
Phenanthrene		97.7	33
Pyrene		30.95	33
	Total SVOCs	304.05	113
Method 8260 (VOC)			
Benzene		110	20
Ethylbenzene		245	48
Toluene		530	66.5
Xylenes		700	180
	Total VOC	1585	314.5

Dewatering System Capacity Density of Water (lb/gal)		8.34
Conversion Factor (lb/g)	0.0022	0.04
Conversion Factor (mg/g)	1000	
Conversion Factor (g/kg)	1000	
Total SVOCs (lb/lb)	0.00030405	
Total VOCs in Feed (lb/lb)	0.001585	
Potential SVOC and VOC		
throughput (lb/lb)	0.00188905	Sum of SVOCs and VOCs in feed
		Based on 40 CFR 61, Subpart FF requirements; Note that carbon actually provides a 99.9% control efficiency if monitored for breakthrough and changed after breakthrough is detected (per carbon system vendors); however, 95% used as a conservative measure in accordance with regulatory
VOC Control Efficiency (%)	95%	requirements.
Thermal Desorption System		
Feed Rate Capacity (tons		Based on system design (range of 18,000 to 20,000,
feed/year)	22500	depending on solids percentage of feed)
Concentration Ratio of		Typical design solids concentration ratio of sludge processed
Dewatering system	4	in dewatering system (pre to post dewatering system)
Dewatering System Feed		
Rate Capacity (tons		Based on system design of thermal desorption system * concentration ratio of dewatering system
feed/year)	90000	(range of 18,000 to 20,000, depending on solids percentage of feed)
Percentage of Volatile		Engineering estimate based on relative non-volatility of material remaining in sludges after
Material Processed Emitted		processing steps prior to dewatering system. Note that most of the oil will be recovered in the
at Dewatering (%)	10%	dewatering and thermal desorption system.
Potential Uncontrolled		
SVOC and VOC emissions		
(tpy)	17.00	
Potential Controlled SVOC and VOC emissions (tpy)	0.85	

BP Products North America, Inc. Page 38 of 42

# **Thermal Desorption System**

The thermal desorption system is a closed system with the exception of vents for the processed solids system, the noncondensible stream that is vented to the system burners, and the burner emissions. Refer to the application for a detailed description.

#### Waste Stream Composition Estimates

Solids (% by weight from the		
dewatering system)	40%	Based on conservative typical design estimates
Water (% by weight from		
dewatering system)	40%	Based on conservative typical design estimates
Oil (% by weight from		
dewatering system)	20%	Based on conservative typical design estimates

#### System Capacity Information

80%	Based on conservative design estimates - 90% recovery is typically expected
20%	Based on conservative design estimates - 10% noncondensibles are typically expected
9000	Based on system design
	Based on system design (range of 18,000 to 22,500, depending on solids percentage of
22500	feed)
	20% 9000

### Noncondensible Hydrocarbons Routed to Burner

Assumes that negligible amounts of organic material will be left in recovered solids after thermal desorption and that all the material that is not recovered is included in the noncondensibles portion. Note that the noncondensible portion will consist of hydrocarbons that do not condense at above 150 to 160 degrees F such as methanes and propanes.

Oil in Feed (tpy)	4500	Percent by weight oil in feed * System Feed Rate Capacity
Noncondensible Portion of		
Oil in Feed (tpy)	900	Percent by weight noncondensible portion * Oil in Feed
VOC Control Efficiency (%)	99.9%	Based on vendor tests for other applications of the thermal desorption system
Potential VOC Emissions		
(tpy)	0.9	Noncondensible Portion of Oil in Feed * (1-VOC Control Efficiency)

Based on the previous experience of the vendor with other waste streams that contain sulfur compounds, hydrogen sulfide in the stream from the thermal desorption unit is typically absorbed in the condensed oil and elemental sulfur typically remains in the solids. The sulfur emissions from the fuel burned in the burner typically are greater than those from the supplemental noncondensible stream.

#### Processed Solids System

It is presumed that negligible amounts of VOC will be emitted from the recovered solids since they have been processed through the thermal desorption system. In addition, the recovered solids system will be enclosed for the rehydration process and routed to a wet scrubber. Therefore, the controlled emissions are presumed to be neglible.

#### **Diesel Fired Burner Emissions**

The thermal desorption system is equipped with two burners that burn distillate fuel. In addition, the noncondensible vapor stream is routed through the burners for destruction of the lighter hydrocarbons that are not recovered in the oil. Note that the noncondensible portion will consist of hydrocarbons that do not condense at above 150 to 160 degrees F such as methanes and propanes.

**Distillate Firing Emissions:** 

Hours of Operation	8760	
Burner Rating (MMBtu/hr)	8	Total maximum rating of two burners
Density of Diesel Fuel (lb/gal)	7.05	
Heating Value of Fuel (Btu/lb)	19,300	From note in AP-42 section 3.3 below table 3.3-1
Heating Value of Fuel (Btu/gal)	137,000	From AP-42 Appendix A, Typical parameters of various fuels
Fuel Consumed (lb/hr)	414.51	
Fuel Consumed (gal/hr)	59	
		Based on maximum burner capacity; Note that 750 to 1000 gallons per day is
Fuel Consumed (gal/day)	1411	the expected usage rate
Fuel Sulfur %	0.05	As required by 40 CFR 80.29(a)(1) - distillate produced by BP Whiting

#### Criteria Pollutants

	NO <sub>x</sub>	со	SO <sub>2</sub>	PM <sub>10</sub> (Filterable)	PM <sub>10</sub> /PM <sub>2.5</sub> (Filterable + Condensable)	voc
AP-42 Emission Factor (lb/kgal)	20	5	7.1	2	3.3	0.2
Emissions (lb/hr)	1.18	0.29	0.42	0.12	0.19	0.01
Emissions (tpy)	5.15	1.29	1.83	0.52	0.85	0.05

#### Other Pollutants

	Lead	Mercury	Beryllium	Benzene*
AP-42 Emission Factor (lb/10^12 Btu)	9	3	3	2.14E-04
Emissions (lb/hr)	0.00	0.00	0.00	<0.01
Emissions (tpy)	0.00	0.00	0.00	<0.01

#### Notes

Emission Factors taken from AP-42 Section 1.3 tables 1.3-1, 1.3-2, 1.3-3 assuming boiler fired by No. 2 oil (9/98).

VOC emission factor is NMTOC factor from AP-42 Section 1.3-3 (9/98).

SO2 emission factor = 142 \* Fuel Sulfur % (AP-42, Section 1.3, Table 1.3-1, 9/98).

PM<sub>10</sub> emission factor is sum of filterable and condensable factors from Tables 1.3-1 and 1.3-2.

PM is assumed to be equal to filterable factor only for purposes of these calculations.

The thermal desorption system will use the existing diesel tank associated with the FBI system. In addition, the thermal desorption system will use less fuel than the existing FBI system has used in the past; therefore, no increases associated with the tank are included.

### Sample Calculation

NOx Emissions (lb/hr) =	8 MMBtu	1000000 Btu	lb	gal	kgal	20 lb	= 1.18 lb/hr
	hr	MMBtu	19300 Btu	7.05 lb	1000 gal	kgal	

<sup>\*</sup>Other pollutant emission factors are from Tables 1.3-9 and 1.3-10. The benzene emission factor is in lb/kgal.

#### **Process Gas Stream Combustion Emissions:**

Note that the distillate fuel use will be adjusted as the noncondensible portion provides heat input capacity such that the maximum rating of the burners will remain at 4 MMBtu/hr each. Therefore, the emissions calculated for the burners should account for all combustion emissions; however the emissions from the combustion of the vapors are calculated below for reference in determining if the emissions are higher when firing process gas in lieu of some of the diesel.

		ingrior writer ming process gue in nea or como er are alcool.
Potential VOC in		
Noncondensible Stream (tpy)	900	
Molar Volume (L/mol)	22.41	Volume of 1 mole of gas, based on the ideal gas law equation at standard conditions
SO2 Molar Weight	64.06	lb/lb-mol or g/mol
VOC Vapor Molar Weight (lb/lb-		
mole)	130	Vapor molecular weight of distillate number 2 from TANKS 4.09d
Conversion Factor (L/cf)	28.32	
Conversion Factor (lb/g)	0.0022	
Total VOC Routed to Burners		
(lb-mole/hr)	1.58	
Converted Molar Volume of		
gas (scf/lb-mol)	359.80	
Total Volume of Organic		
Vapors Combusted (MMscf/hr)	5.69E-04	Based on the total VOC combusted per hour multiplied by the molar volume of the gas
Total Volume of Vapors		
Combusted (MMscf/yr)	4.98E+00	Based on the total VOC combusted per year multiplied by the molar volume of the gas
Higher Heating Value of		
Refinery Fuel Gas		Conservatively assumes that the gas has a similar heating value to refinery fuel gas,
(MMBtu/MMscf)	1200	although the heating value will vary.
Higher Heating Value of		This is used to convert the natural gas emission factors per footnote a in Table 1.4-1 of AP-
Natural Gas (MMBtu/MMscf)	1020	42 Section 1.4.
		Based on the average hydrogen sulfide content of the refinery fuel gas from 2003-2004.
		This conservatively assumes the same H2S concentration as refinery fuel gas; however, the
		H2S is not expected to be present in significant quantities in the noncondensible stream
Sulfur Concentration (ppm)	46.03	since it should be absorbed in the oil condensing phase.

	NO <sub>x</sub>	CO	SO <sub>2</sub>	PM/PM <sub>10</sub> /PM <sub>2.5</sub>
Emission Factor based on Natural Gas				
(lb/MMscf)	100	84	see below	7.6
Burner Exhaust Emissions (lb/hr)	0.07	0.06	0.06	<0.01
Burner Exhaust Emissions (tpy)	0.29	0.25	0.28	0.02

Converted Flow Rate to		
Burners (MMscf/hr)	0.008	Conservatively based on natural gas heat input and the maximum capacity of the burner
SO2 Emission Rate (lb/hr)	0.06	
SO2 Emission Rate (tpy)	0.28	

The emissions associated with the diesel burners are higher than emissions when burning process gas; therefore, the diesel burner emissions will be used for potential emissions estimates.

Notes

Emissions factors for  $NO_X$ , CO,  $PM_{10}$  are from AP-42 Section 1.4 tables 1.4-1 and 1.4-2 (7/98) assuming combustion similar to natural gas. PM is assumed to be equal to  $PM_{10}$  and  $PM_{2.5}$  or the purposes of these calculations.

Molar volume for VOC and SO2 calculated using ideal gas law at standard temperature and pressure.

These calculations are conservative as the noncondensible stream is not likely to contain as much hydrogen sulfide as the refinery fuel gas.

Note that it is presumed that the sulfur compounds in the noncondensible stream will mostly be H2S. Other reduced sulfur compounds that could be formed in the thermal desorption unit have similar boiling points to the hydrocarbons that are condensed and recovered, and these other sulfur compounds are expected to condense in the oil phase with the hydrocarbons.

# **Fugitive Emission Factors**

	EPA Refinery Average Emission		EPA Refine	ry SCREENING	EPA Refinery SCREENING		
	Factors		Emission F	actors - LEAK	Emission Factors - NO LEAP		
Equipment/Service	Kg/hr/source	lbs/hr/source	Kg/hr/source	lbs/hr/source	Kg/hr/source	lbs/hr/source	
Valves							
Gas/Vapor	0.0268	0.059083816	0.2626	0.5789	0.0006	0.0013	
Light Liquid	0.0109	0.024030358	0.0852	0.1878	0.0017	0.0037	
Heavy Liquid	0.00023	0.000507063	0.00023	0.00051	0.00023	0.00051	
Pumps							
Light Liquid	0.114	0.25132668	0.437	0.963	0.012	0.0265	
Heavy Liquid	0.021	0.04629702	0.3885	0.8565	0.0135	0.02976	
Flanges							
Gas/Vapor	0.00025	0.00055	0.0375	0.0827	0.00006	0.00013	
Light Liquid	0.00025	0.00055	0.0375	0.0827	0.00006	0.00013	
Heavy Liquid	0.00025	0.00055	0.0375	0.0827	0.00006	0.00013	
Compressors	0.636	1.40214	1.608	3.545	0.0894	0.1971	
Relief Valves	0.16	0.35274	1.691	3.728	0.0447	0.0985	
Open-ended Lines	0.0023	0.00507	0.01195	0.02635	0.0015	0.0033	
Sampling Connections	0.015	0.03307	0.0375	0.0827	0.00006	0.00013	

#### Reference:

A Factors are taken from EPA Document EPA-453/R-95-017, Nov. 1995, Table 2-2, Page 2-13.

# Fugitive Emission Calculations for Dewatering and Thermal Desorption System

It is conservatively assumed that the components are in light liquid or vapor service, although the components may be in heavy liquid service. Only the new components associated with the new portions of the sludge handling system are included here.

LDAR Program: Monitoring per Consent Decree<sup>1</sup>;

Factor Type: Refinery

Screening

(EPA Emission Factors EPA-453/R-95-017, Table 2-6)

Annual Hours of Service: 8760

	Estimated Component	EPA 'Refinery Screening' Factors LEAK	EPA 'Refinery Screening' Factors NO LEAK		Maximum Uncontrolled Emission Rate	LD&R Control	Percent in VOC	Total VOC Emissions
Component Type	Count	(lb/hr/component)	(lb/hr/component)	Percent Leak	(lbs/hr)	Efficiency <sup>2</sup>	Service	(Tons/yr)
Valves								
Gas/Vapor	22	0.5789	0.0013	2.0%	0.2827	95%	100%	0.06
Light Liquid	20	0.1878	0.0037	2.0%	0.1476	95%	100%	0.03
Heavy Liquid	0	0.00051	0.00051	2.0%	0.0000	30%	100%	0.00
Pumps								
Light Liquid	10	0.9630	0.0265	2.0%	0.4523	80%	100%	0.40
Heavy Liquid	0	0.8565	0.02976	2.0%	0.0000	30%	100%	0.00
Flanges								
Gas/Vapor	48	0.0827	0.00013	0.3%	0.0181	30%	100%	0.06
Light Liquid	60	0.0827	0.00013	0.3%	0.0227	30%	100%	0.07
Heavy Liquid		0.0827	0.00013	0.3%	0.0000	30%	100%	0.00
Compressors	0	3.545	0.197	2.0%	0.0000	0%	100%	0.00
Relief Valves	10	3.728	0.099	2.0%	1.7109	100%	100%	0.00
Open-ended Lines	0	0.026	0.003	2.0%	0.0000	0%	100%	0.00
Sampling Connections	2	0.083	0.00013	2.0%	0.0036	0%	100%	0.02
						Total VOC E	missions (lbs/day):	3.46
						Total VOC E	missions (tons/yr):	0.63

<sup>&</sup>lt;sup>1</sup> United States, et.al v. BP Exploration & Oil, et.al., Northern District of Indiana, Hammond Division, Civil Action No. 2:96 CV 095 RL

30% control estimate per TCEQ Guidance "Air Permit Technical Guidance for Chemical Sources: Equipment Leak Fugitives" (October 2000).

**B** Factors are taken from EPA Document EPA-453/R-95-017, Nov. 1995, Table 2-6, Page 2-20.

<sup>&</sup>lt;sup>2</sup> LD&R control efficiency for pumps and valves in gas and light liquid service are 95% and 80%, respectively based on a 500 ppmv leak definition for valves and 2000 ppmv compared to the 10,000 leak definition basis for screening factors (i.e., (1-500//10,000 = 95%) and (1-2,000/10,000) = 80%) AVO monitoring equivalent to 30% control is applied to all flanges and heavy liquid valves and pumps.